

Computer Program for Calculating Propagation Loss into the Shadow Zone

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13. ABSTRACT

A computer program has been developed for calculating the propagation loss of underwater sound into the region of the shadow zone. The calculations are based on a composite propagation scattering model. The computer program has been written partly in FORTRAN IV and partly in NELIAC. Copies of this program are available to interested parties.

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ABSTRACT

A computer program has been developed for calculating the propagation loss of underwater sound into the region of the shadow zone. The calculations are based on a composite propagation scattering model. The computer program has been written partly in FORTRAN IV and partly in NELIAC. Copies of this program are available to interested parties.

PROBLEM STATUS

This concludes the work on this problem, which was terminated June 30, 1969. Unless otherwise notified, this problem will be considered closed 30 days after the issuance of this report.

AUTHORIZATION

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COMPUTER PROGRAM FOR CALCULATING PROPAGATION LOSS INTO THE SHADOW ZONE

INTRODUCTION

A program named Assured Range Studies was carried on by the Acoustic Warfare (formerly Techniques) Branch of the Acoustics Division. One of the results of the Assured Range Studies was the development of a means of computing the propagation loss of acoustic energy in the ocean from a source in the surface layer to any point below the layer. The purpose of this report is to describe the computer program for the calculation of this propagation loss.

It is a common occurrence for the ocean to develop a layer of water which is virtually isothermal. This layer of almost constant temperature starts just below the ocean surface and can extend downward for several hundred feet. The sound speed gradient in the isothermal layer is positive in the downward direction due to the increase in the hydrostatic water pressure with depth. Immediately below the layer the sound speed gradient is negative. This is caused by the relatively rapid decrease of water temperature with depth. Sound propagation in the layer, or surface duct as it is also called, is usually favorable.

For a sound source in the surface layer there exists a limit ray. The limit ray is the ray which leaves the source at an angle such that it crosses the bottom boundary of the duct at grazing incidence. Ray theory predicts no sound propagation below the duct boundary beyond the point of grazing incidence of the limit ray. This region is the shadow zone.

Experience has shown that the shadow zone is insonified, and the Assured Range Studies proposed a propagation scattering model for determining sound intensity there. Specifically, it was asserted that the principal mechanism for insonifying the region is the scattering of acoustic energy by the rough, irregular sea surface.

This propagation scattering model requires the knowledge of only those parameters that can be measured. The parameters are the sound speed variation with depth, wind speed, depth of the isothermal duct, depth of the sound source, range between source and receiver (or target), and depth of the receiver. (The terms *receiver* and *target* will be used interchangeably throughout this report.) However, the calculation of propagation loss is so intricate and lengthy that it is made practicable only by means of a digital computer. A brief description covering the important points of the propagation scattering model is given below.

DESCRIPTION

The propagation scattering model asserts that acoustic rays diverge from the source, where they are refracted in accordance with the sound speed gradient, and are then reflected and/or scattered from the surface into the shadow zone. The scattering occurs from an area between source and receiver. (It is assumed that backscattering is unimportant, and areas beyond the receiver make no significant contribution to the signal strength at the receiver. Also, there is no contribution by sound reflected from the ocean bottom.) The scattering strength of any point on the surface is a continuous

function of position with respect to the source and the receiver. But since the scattering cannot be computed over any continuous extent from a practical standpoint, the surface of the ocean between source and receiver is divided into a number of elementary scattering areas, in this case squares all of the same size. Such a division is diagrammed in Fig. 1, where S is the source and T is the target. The scattering strength is computed at the center of each of the elementary scattering areas, and it is assumed constant over the entire square.

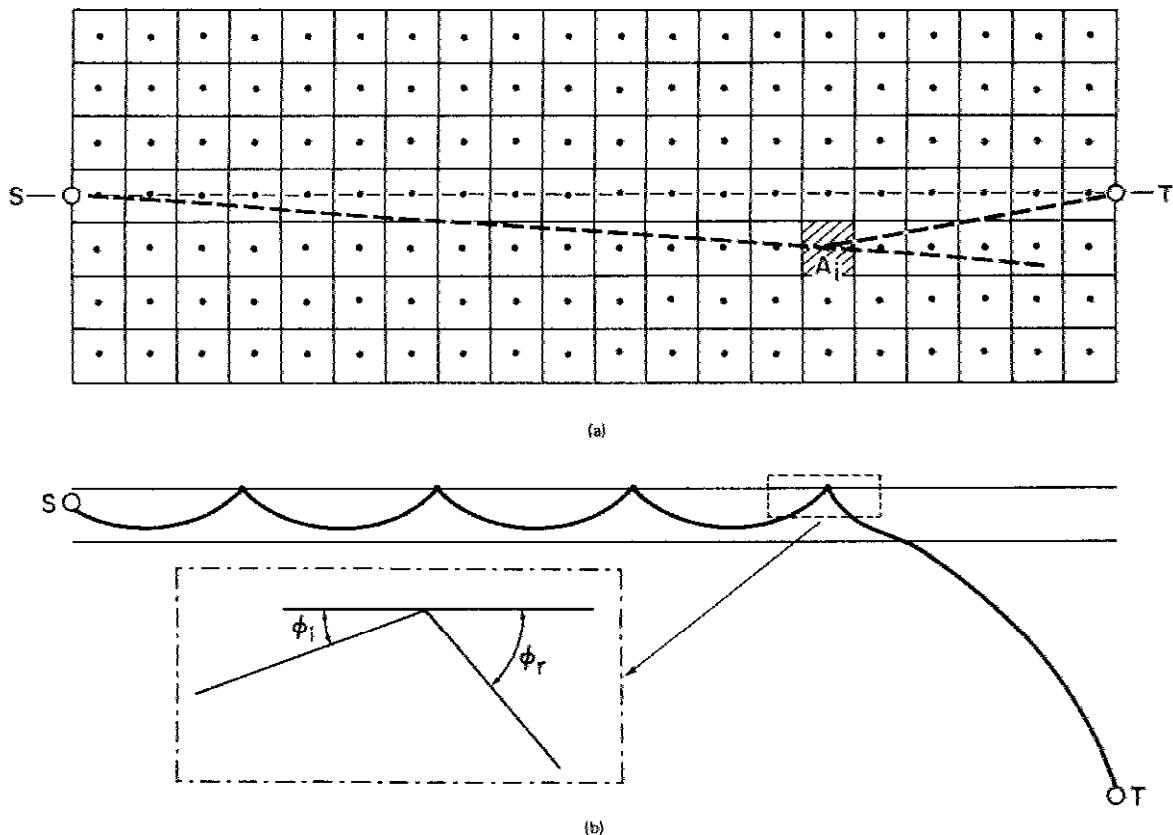


Fig. 1 - Diagram of scattered ray, (a) ocean surface divided into elementary scattering areas, (b) geometry of scattered ray

With the division of the ocean surface into the elementary scattering areas, a set of individual ray paths is thus defined. The individual ray path is the path from the source to the center of any scattering area and from there to the receiver. For the i th square the propagation loss H_i in decibels is computed and displayed in the computer output. Each value of H_i is converted to its equivalent intensity, and all the intensities are added together. From the sum of the equivalent intensities the total propagation loss is determined.

The number of ray paths or the total extent of the scattering surface considered is dependent on the limits set for scattering strength and the values of H_i for elementary scattering areas lying on the central axis between source and receiver. The scattering strength of a scattering area decreases as areas further from the central axis are considered. When the scattering strength falls below -60 dB, areas further off the central axis are not considered. The error caused by not considering a larger area is a small

fraction of a decibel. The computations start by considering the ocean surface at the receiver end of the propagation path and "working" back toward the source. The values of H_i for the elementary scattering areas reach a maximum, usually within 1000 yd of the target. That there is a maximum value for H_i is a conclusion made after several preliminary calculations had been made. When H_i for a square, whose center lies directly on the center line, is less than -150 dB, the computation of H_i for any other area is terminated and the summation of all the intensity equivalents of the H_i 's is made. (Again, here, errors due to truncation are small.) This final value of H is the propagation loss to a point in the shadow zone, i.e., at the target. The signal strength at the receiver is due to the scattered field. This theory and the program do not consider the "direct" field that would be encountered in the duct, and the target below the duct receives only the energy in the scattered field. The computer printout also includes the scattering strength of each scattering area and the angle of arrival each ray makes with the target.

The propagation loss H_i , in decibels, of each ray is the sum of four terms, as given in Eq. (1).

$$H_i = TL_{1i} + 10 \log_{10} S_{si} + 10 \log_{10} A_i + TL_{2i}. \quad (1)$$

(The subscript i in Eq. (1) will not be used in the following discussion.) The loss TL_1 is the loss along the ray from the source to the scattering area. To compute this loss, the AMOS (1) formulations were used plus a surface-coupled loss, suggested by M. Schulkin (2), that the ray suffers on scattering from the surface.

The quantity S_s of Eq. (1) is the scattering coefficient of the scattering area, and $10 \log S_s$ is called the scattering strength. S_s is computed using the scattering model developed by Beckmann-Spizzichino (3). Their development includes scattering from a moderately rough to rough, irregular surface depending on acoustic frequency, standard deviation of wave height, and the angle at which the target "sees" the scattering area. The elementary scattering area A is a square of 50 yd on a side.

The quantity TL_2 is the propagation loss the ray suffers from the area of scattering to the target. The loss TL_2 is found by a ray-tracing method outlined by Stewart (4). From bathymetric and salinity data the sound speed for any depth is computed using Wilson's (5) equations. Stewart's method generates a sound speed profile that is not only continuous at the layer boundaries, but the first derivative of the sound speed with respect to depth is also everywhere continuous. This method is adequate for computing TL_2 because the sound speed structure can be accurately portrayed below the duct as well as within the duct. In the region through which TL_1 is computed, the sound speed is a linear function of depth because of the isothermal water.

GUIDE FOR USERS

The input parameters for this computer program are all either chosen or measured except for PHISUB1 (see list below). These values are listed below with their equivalent FORTRAN designations.

This information goes on one data card which is read by a FORTRAN read instruction. This single data card is to be followed by the sound speed profile. The curvilinear sound speed profile is generated by another computer program SOUNDSPEED which is in the NELIAC compiler language. The inputs for the sound speed profile require either depth sound speed pairs or temperature and salinity data and their corresponding depths.

Preliminary calculations showed that the Beckmann-Spizzichino scattering model is quite insensitive to small changes of small angles of PHISUB1 (ϕ_i). Even for the deepest

<u>Definition</u>	<u>FORTRAN Designation</u>
Channel depth (yd)	HC
Receiver depth (yd)	RDEPTH
Angle of incidence of ray at surface (degrees)	PHISUB1
Wind (knots)	W
Acoustic frequency (kHz)	FREQ
Value of linear gradient in duct (1/sec)	GC
Range between source and target (yd)	RINITIAL
Source depth (yd)	ZSUB0
Surface temperature ($^{\circ}$ F)	TEMP

surface ducts PHISUB1 will be about 3.5 degrees at most. Therefore PHISUB1 can be arbitrarily set to any small angle less than 3.5 degrees. A value of 2 degrees was used by the author.

FLOW DIAGRAM

The flow diagram of Fig. 2 shows the general computation scheme. Figs. 3 through 6 are the major subroutines except for subroutines INITPTOP and PTOP. These latter two subroutines are in the NELIAC-N compiler language. Their purpose will be noted below.

The first five operations after start given in Fig. 2 read in all of the data except for the sound speed profile, print this data as an output, calculate several constants as noted in operations numbered 4 and 5, divide the ocean surface as illustrated in Fig. 1, and compute all ranges for the determinations of TL_1 and TL_2 . Subroutine DATA, which computes the ranges for TL_1 and TL_2 , is diagrammed in Fig. 3.

Subroutine INITPTOP calls subroutine RDPROFILE, which reads in and stores the sound speed profile. INITPTOP also calculates a table of sound speeds for use by PTOP. The quantities FLAG, I, MX, and N are counting and controlling indexes. The subroutine PTOP computes the propagation loss TL_2 , the angle of scattering from the surface and the angle of arrival at the target. PTOP finds the solution ray subject to the constraints of the problem. The constraints placed on the ray are horizontal range, depth of the source (which is the surface), depth of the target, and the sound speed gradient. The angle of scattering from the surface comes about by selecting only that ray that leaves the surface such that it will arrive at the target, given those constraints. This angle is required for subroutine SSS, and it is designated ϕ_s in Fig. 1.

The subroutine SSS computes the scattering strength $10 \log_{10} S_s$ of Eq. (1) and subroutine CMPUTE H calculates TL_1 and makes the addition of the quantities indicated in Eq. (1). Subroutine TABLE(MX) prints the output of the program in tabular form. The output table format displays the quantities H, $10 \log_{10} S_s$, and ANGRCVR (angle of arrival at the target) for each elementary scattering area. The numbers are arranged on

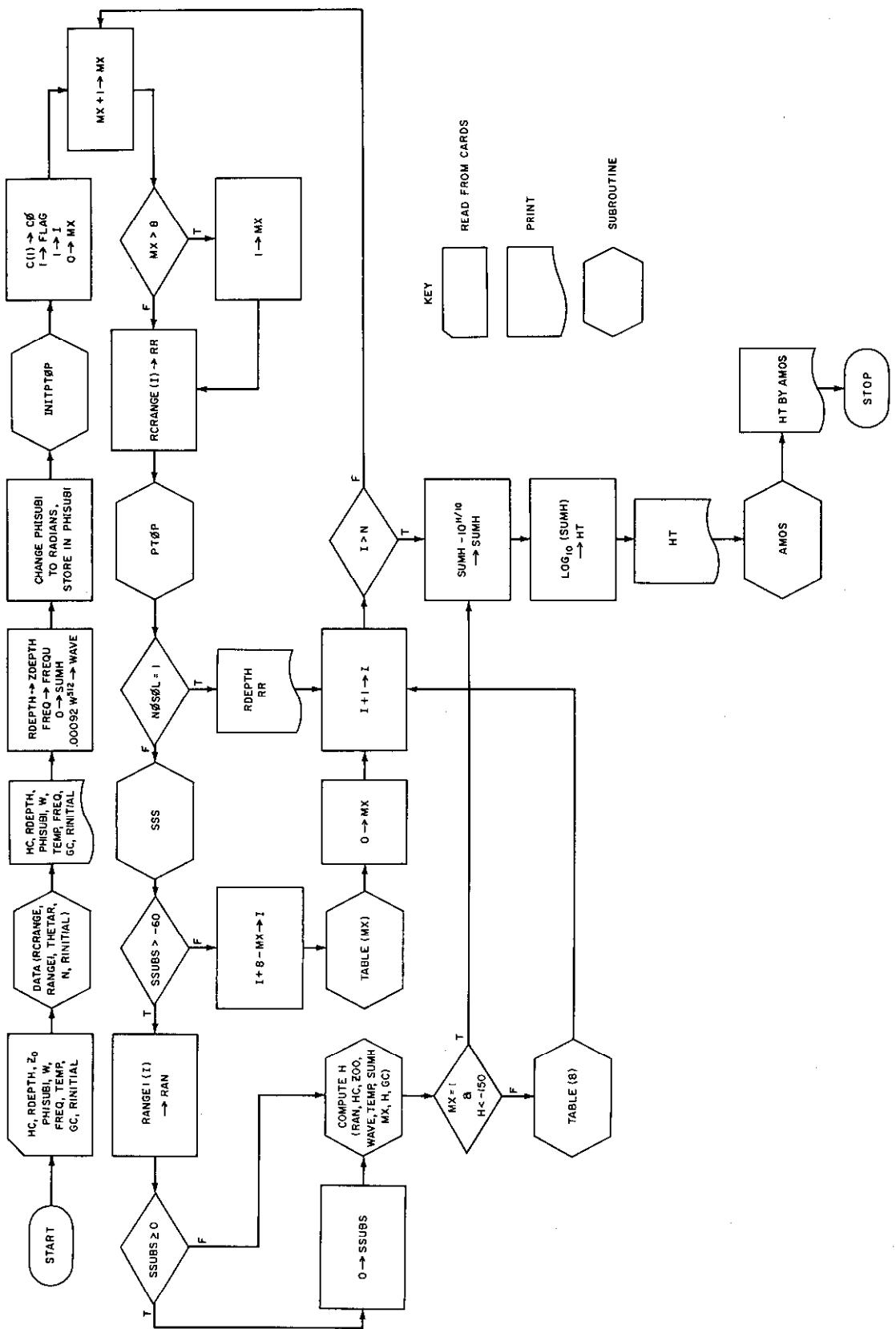


Fig. 2 - Flow diagram of main program for SURFSCAT

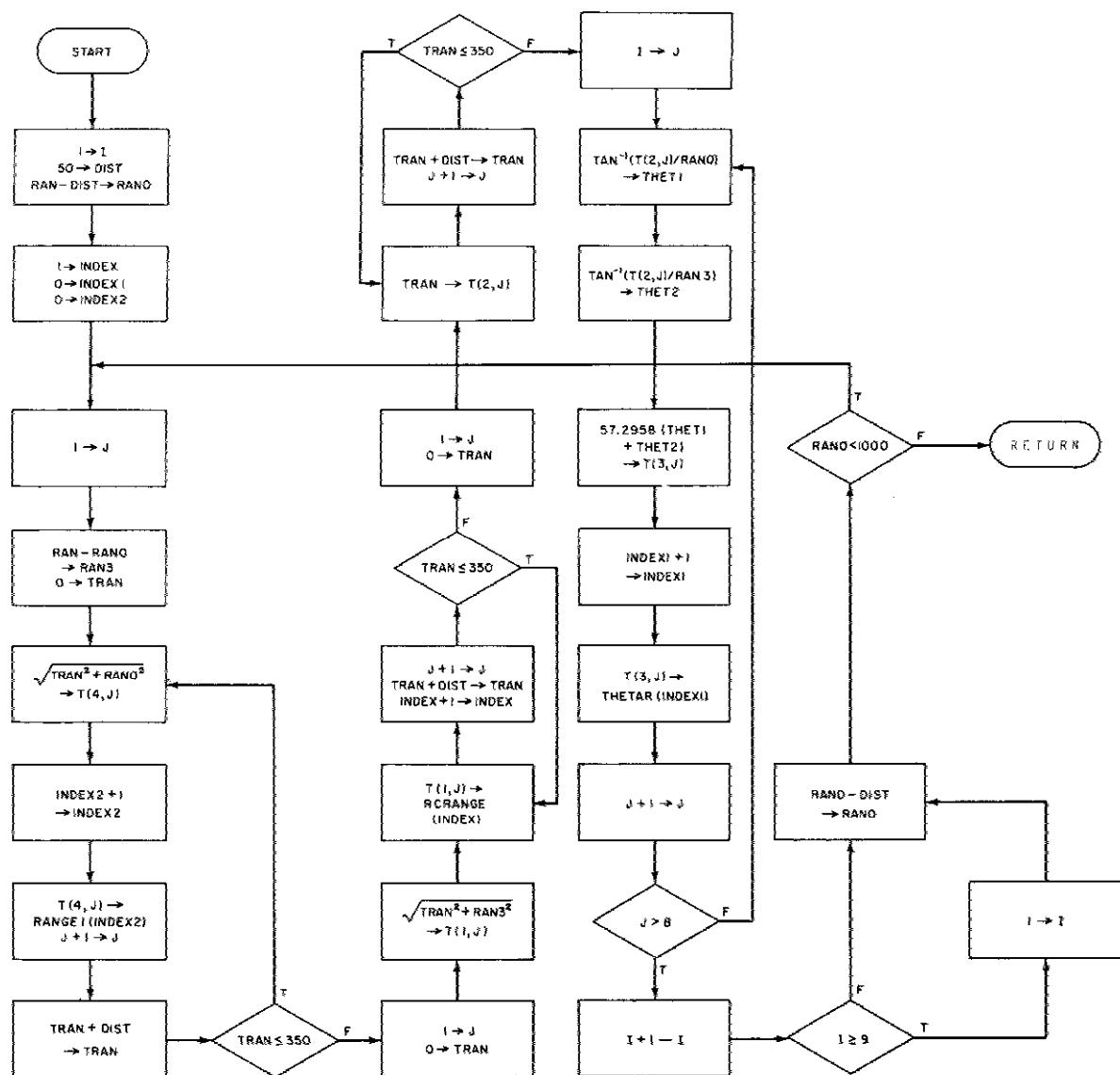


Fig. 3 - Flow diagram for range calculation for computing TL_1 and TL_2 and for calculation of θ_r

the page to correspond to the relative location of their position on the sea surface. But since the manner in which the surface is divided gives asymmetry with respect to the axis connecting source and target, only those values to one side (the right one) of this axis are printed.

The main program SURFSCAT computes the effective intensity for each ray, normalized to the source level of 1 yd, by taking $\log_{10}^{-1}(H_i/10)$. These effective intensities are summed, and then the total propagation loss between the source and the target is computed as $10 \log_{10}$ of the summed effective intensities.

Subroutine AMOS computes this same quantity using only the AMOS formulations throughout the entire extent of the transmission path.

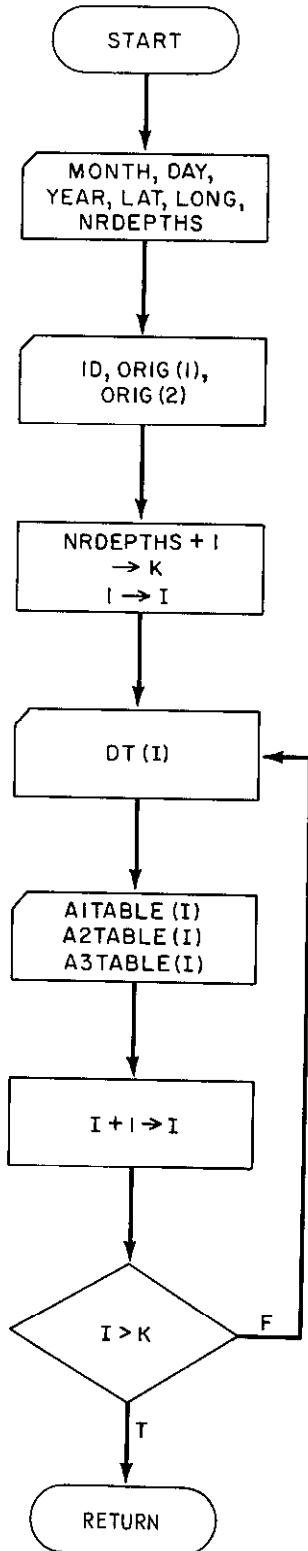
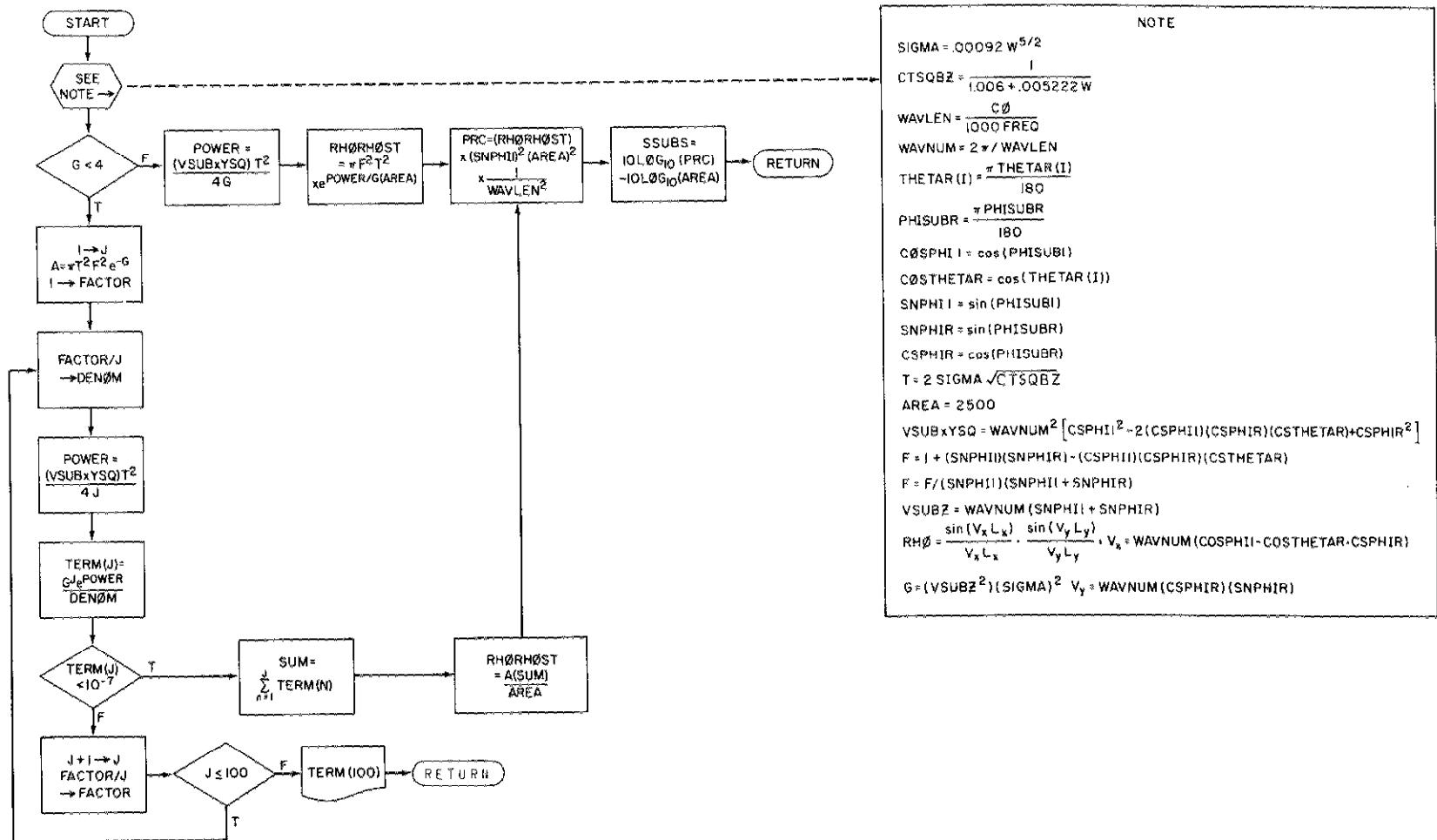


Fig. 4 - Flow diagram
for reading the sound
velocity profile

Fig. 5 - Flow diagram for calculation of $10 \log_{10} S_s$

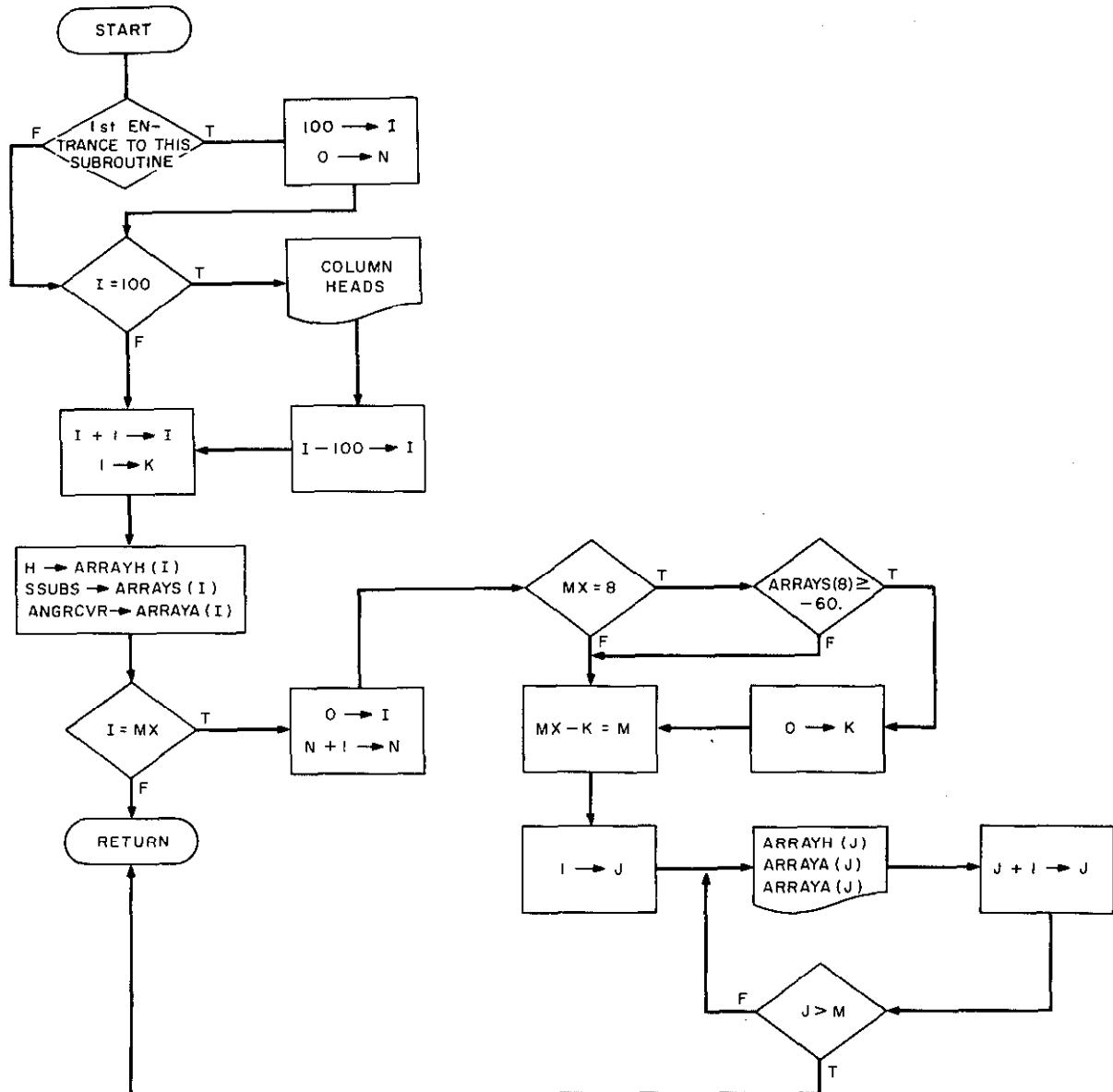


Fig. 6 - Flow diagram of printout

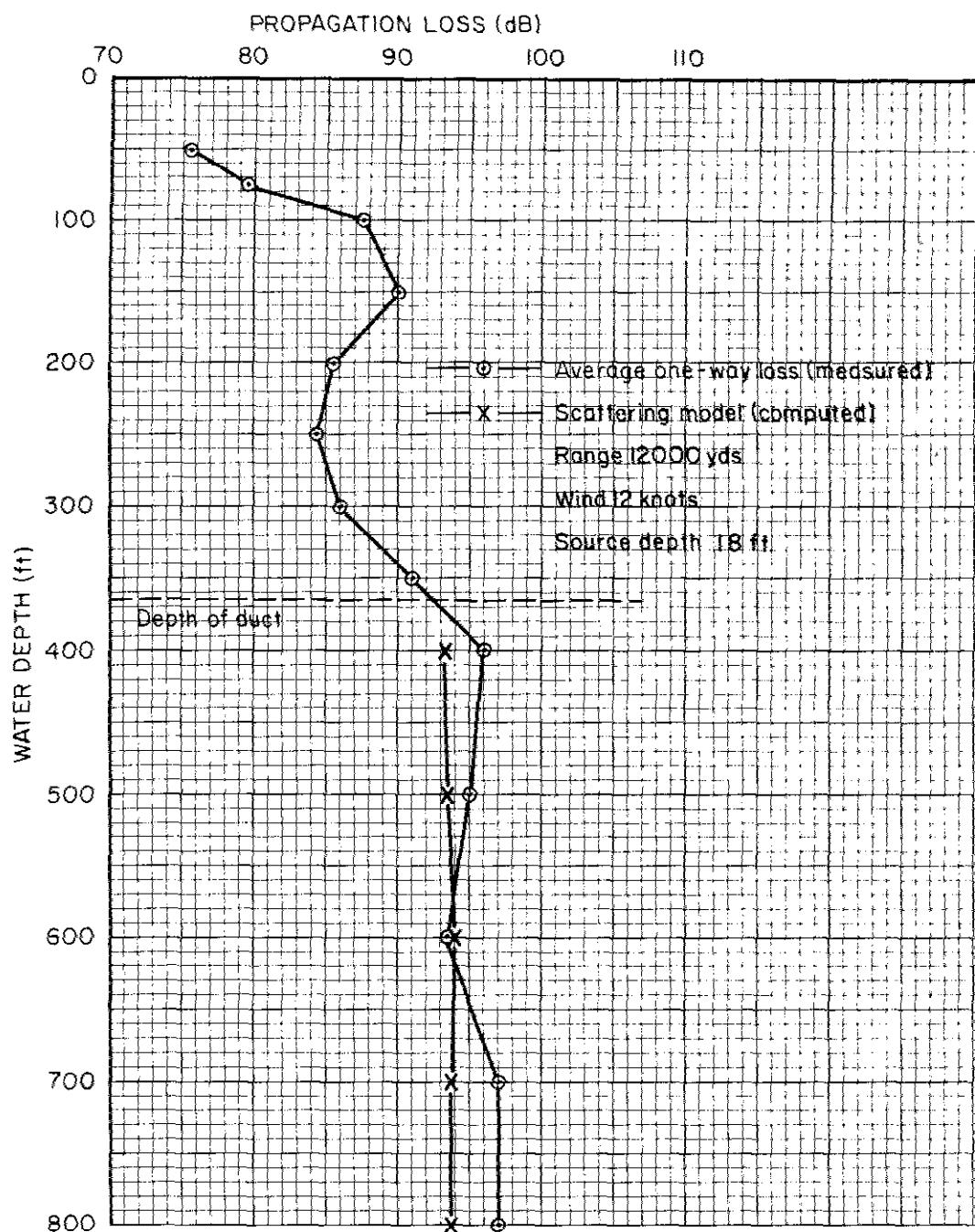


Fig. 7 - Propagation loss vs depth

A complete program listing is given in the Appendix. This computer program has been run repeatedly using field data collected during experiments at sea. These data were restricted to one frequency, but there were variations of range, target depth, surface duct depth, sound speed profile, and wind speed. The difference between computed and measured values of propagation loss never exceeded ± 3.5 dB, where the measured value was based on the average loss for 20 to 30 pings. Shown in Fig. 7 are some typical propagation loss measurements for various depths for a constant range of 12,000 yards. The source depth is about 6 yd.

REFERENCES

1. March, H.W., Jr., and Schulkin, M., "Report on the Status of Project AMOS," USL Report 255A, May 9, 1967
2. Schulkin, M., J. Acoust. Soc. Amer. (Letter to the Editor), 44:1152-1154 (1968)
3. Beckmann, P., and Spizzichino, A., "The Scattering of Electromagnetic Waves from Rough Surfaces," New York:Pergamon, 1963
4. Stewart, K.R., J. Acoust. Soc. Amer. 38:339-347 (1965)
5. Wilson, W.D., J. Acoust. Soc. Amer. 32:641-644 (1960)

Appendix A
Program Listing for SURFSCAT

```

PROGRAM SURFSCAT                                     SUR00100
C
C SURFSCAT COMPUTES THE PROPAGATION LOSS OF ACOUSTIC ENERGY EMITTED   SUR00200
C FROM A SOURCE IN THE SURFACE DUCT SCATTERED INTO THE SHADOW ZONE.   SUR00300
C THIS LOSS IS A FUNCTION OF WIND VELOCITY, TEMPERATURE, SOURCE AND   SUR00400
C RECEIVER DEPTHS, DUCT DEPTH, FREQUENCY, RANGE, AND THE SOUND VELOCITYSUR00500
C PROFILE.                                                 SUR00600
C
C THE SCATTERING SURFACE IS DIVIDED INTO SQUARES OF EQUAL SIZE. THE   SUR00700
C SCATTERING STRENGTH IS COMPUTED AT THE CENTER OF EACH SQUARE, AND IT   SUR00800
C IS ASSUMED CONSTANT OVER THE ENTIRE SQUARE.           SUR00900
C
C
C DIMENSION RCRANGE(3000),THETAR(3000) ,RANGE1(3000)          SUR01300
C COMMON/SSS DATA/ANGSRC,ANGRCUR,PLOSS,RR,RDEP(H,FREQ,NOSOL,FLAG, SUR01400
C 100,SSUBS
C COMMON/SSS PRAM/W,PHISUB1,THETAR,I                      SUR01500
C COMMON/A/H
C COMMON/PROFILE/MONTH,DAY,YEAR,LAT,LONG,TD,ORIG(2),NRDEPTH,SRT,   SUR01700
C *          DOND,MTHD,
C DT(800), C(800), A1TABLE(800), A2TABLE(800), A3TABLE(800)      SUR01800
C COMMON/ANDY/HC, ZSRC, ZDEPTH, RINITIAL, FREQ, WAVE, TEMP        SUR01900
C
C RCRANGE(I) IS THE STRAIGHT LINE DISTANCE BETWEEN THE I TH SCATTERING SUR02400
C POINT AND THE POINT ON THE SURFACE DIRECTLY ABOVE THE RECEIVER    SUR02500
C (POINT A).                                              SUR02600
C
C RANGE1(I) IS THE DISTANCE BETWEEN THE SOURCE AND THE I TH SCATTERING SUR02800
C POINT.                                                 SUR02900
C
C THETAR(I) IS THE ANGLE BETWEEN THE VECTOR FROM THE SOURCE TO THE I THSUR03100
C SCATTERING POINT AND THE VECTOR FROM THE I TH SCATTERING POINT TO   SUR03200
C POINT A.                                              SUR03300
C
C RDEPTH IS THE RECEIVER DEPTH IN YARDS.                   SUR03400
C
C HC IS THE CHANNEL DEPTH IN YARDS.                     SUR03500
C
C PHISUB1 IS THE ANGLE OF INCIDENCE A RAY MAKES WITH A SCATTERING SUR03600
C POINT. IT IS ASSUMED CONSTANT FOR ALL RAYS AND SCATTERING          SUR03700
C POINTS (USUALLY ABOUT 2 DEGREES).          SUR03800
C
C W IS WIND SPEED IN KNOTS.                         SUR03900
C
C FREQ IS THE FREQUENCY OF THE ACOUSTIC SIGNAL IN KHZ.          SUR04000
C
C GC IS THE SOUND VELOCITY GRADIENT IN THE DUCT (A CONSTANT BY      SUR04100
C DEFINITION OF THE DUCT) IN 1/SEC'S.          SUR04200
C
C RINITIAL IS THE DISTANCE BETWEEN THE SOURCE AND POINT A.        SUR04300
C
C ZSUB0 IS THE DEPTH OF THE SOURCE IN YDS.                   SUR04400
C
C TEMP IS THE TEMPERATURE IN THE DUCT (ASSUMED CONSTANT).        SUR04500
C
C     READ 1, HC, RDEPTH, PHISUB1, W, FREQ, GC, RINITIAL, ZSUB0, TEMP  SUR04600
C     1 FORMAT(9F8)
C

```

```

C DATA COMPUTES THE VALUES OF RCRANGE(I), THETAR(I), RANGE1(I), AND SUR05900
C N, WHERE N IS THE TOTAL NUMBER OF SCATTERING POINTS TO BE CONSIDERED. SUR06000
C SUR06100
C CALL DATA(RCRANGE,RANGE1,THETAR,N,RINITIAL) SUR06200
PRINT 9 SUR06300
9 FORMAT(1X*INPUT DATA---*/)
PRINT 10, HC, RDEPTH, PHISUR1, W, TEMP, FREQ, GC, RINITIAL SUR06400
10 FORMAT(5X*CHANNEL DEPTH*5X*RECEIVER DEPTH*5X*PHISUB1*5X*W*8X*TEMP*SUR06600
1 10X*FREQ*5X*GAMMA CONSTANT*5X*INITIAL RANGE*/ SUR06700
25X,F10.3,10X,F10.3,3X,F6.3,5X,F6.3,5X,F8.3,3X,F10.5,10X, SUR06800
3F10.3//)
ZDEPTH = RDEPTH SUR06900
FEQU = FREQ SUR07000
SUMH = 0 SUR07100
WAVE = ,00092*W**(./.2.) SUR07200
PI = 3.1415926535 SUR07300
CON = PI/180.0 SUR07400
PHISUB1 = PHISUB1*CON SUR07500
SUR07600
SUR07700
C INITPTOP IS A NELIAC SUBPROGRAM WHICH CALLS RDPROFILE AND RETURNS SUR07800
C DATA FOR PTOP. RDPROFILE READS THE SOUND SPEED PROFILE WHICH MAY SUR07900
C BE GENERATED BY SOUND SPEED AVAILABLE THROUGH KEN MORIN, NRL. SUR08000
SUR08100
C CALL INITPTOP SUR08200
CG = C(1) SUR08300
FLAG = 1.0 SUR08400
MX = 0 SUR08500
SUR08600
C THE FOLLOWING LOOP COMPUTES THE TOTAL SCATTERING LOSS FROM SOURCE TO SUR08700
C RECEIVER FOR EACH SCATTERING POINT IN DB (H), THE SCATTERING SUR08800
C STRENGTH OF EACH SCATTERING POINT IN DB (10LOG(SSURS)), AND THE SUR08900
C ANGLE OF INCIDENCE OF THE RAY FROM EACH SCATTERING POINT AT THE SUR09000
C RECEIVER (ANGRCVR) IN DEGREES AND PRINTS THESE OUT IN TABULAR FORM. SUR09100
SUR09200
C DO 50 I=1,N SUR09300
MX = MX + 1 SUR09400
IF (MX.GT.8) MX = 1 SUR09500
RR = RCRANGE(I) SUR09600
SUR09700
C PTOP IS A NELIAC SUBPROGRAM WHICH COMPUTES THE PROPAGATION LOSS SUR09800
C FROM A SCATTERING POINT TO THE RECEIVER (TL2) AND THE ANGLE OF SUR09900
C DEPARTURE OF THE SCATTERED RAY FROM A SCATTERING POINT (PHISUBR). SUR10000
SUR10100
C CALL PTOP SUR10200
IF (NOSPL.EQ.1) PRINT 30,RDEPTH,RR SUR10300
IF (NOSPL.EQ.1) GO TO 50 SUR10400
30 FORMAT(20X,*THERE IS NO SOLUTION FOR THIS DEPTH AND RANGE*,5X,
* F7.2,5X,F7.2//)
SUR10500
SUR10600
C SSS COMPUTES THE SCATTERING STRENGTH AT THE CENTER OF ONE OF THE SUR10700
C SCATTERING AREAS. SUR10800
SUR10900
SUR11000
C CALL SSS SUR11100
IF (SSURS.GT.-60.0) GO TO 40 SUR11200
ADD = (R-MX) SUR11300
I = I + ADD SUR11400
SUR11500
C

```

```

C TABLE PRINTS OUT VALUES OF H, 10LOG(SSUBS), AND ANGRCVR IN
C TABULAR FORM.
C
C      CALL TABLE(MX)
C      MX = 0
C      GO TO 50
C      40 RAN = RANGE1(I)
C
C      COMPUTE H COMPUTES THE SCATTERING LOSS FROM THE SOURCE TO A
C      SCATTERING POINT (TL1), H AND SUMS THE EQUIVALENT INTENSITIES,
C      10**((H/10))
C
C      CALL COMPUTE H(RAN, HC, ZSUB00, WAVE, TEMP, SUMH, MX, H, GC)
C      IF(MX,ER,1,AND,H,LT,-150.0) GO TO 55
C      CALL TABLE(8)
C      50 CONTINUE
C      55 SUMH = SUMH - 10**((H/10,0))
C      HT IS THE TOTAL PROPAGATION LOSS FOR ALL OF THE RAYS TRACES,
C      HT = 10*ALOG10(SUMH)
C      PRINT 60, HT
C      60 FORMAT(//20X* THE TOTAL PROPAGATION LOSS (HT) IS *F10.3*)
C
C      AMOS COMPUTES ANOTHER VALUE FOR HT USING THE AMOS FORMULATIONS.
C
C      CALL AMOS
C      END

```

SUR11600
SUR11700
SUR11800
SUR11900
SUR12000
SUR12100
SUR12200
SUR12400
SUR12500
SUR12600
SUR12700
SUR12800
SUR12900
SUR13000
SUR13100
SUR13200
SUR13300
SUR13400
SUR13500
SUR13600
SUR13700
SUR13800
SUR13900
SUR14000
SUR14100
SUR14200

```

      SUBROUTINE RDPROFILE
C
C      RDPROFILE READS THE SOUND SPEED PROFILE WHICH MAY BE GENERATED BY
C      SOUND SPEED AVAILABLE THROUGH KEN MORIN, NPL.
C
C      COMMON/RDPROFILE/MONTH,DAY,YEAR,LAT,LONG,TD,ORIG(2),NRDEPTHS,
C      *BT,DONG,MTHD,
C      1DT(800), C(800), A1TABLE(800), A2TABLE(800), A3TABLE(800)
C      1 READ 2,MONTH,DAY,YEAR,LAT,LONG,TD,ORIG(1),ORIG(2),NRDEPTHS
C      2 FORMAT(1X,I3,1X,I3,1X,I6,1X,F8,1X,F9,1X,A8,1X,2A8/15)
C      K=NRDEPTHS+1
C      5 READ 6,(DT(I),I=1,K)
C      6 FORMAT(4E18.9)
C      READ 6,(C(I),I=1,K)
C      READ 6,(A1TABLE(I),I=1,K)
C      READ 6,(A2TABLE(I),I=1,K)
C      READ 6,(A3TABLE(I),I=1,K)
C      END

```

RDP 0100
RDP 0200
RDP 0300
RDP 0400
RDP 0500
RDP 0600
RDP 0700
RDP 0800
RDP 0900
RDP 1000
RDP 1100
RDP 1200
RDP 1300
RDP 1400
RDP 1500
RDP 1600
RDP 1700
RDP 1800

```

SUBROUTINE SSS          SSS 0100
C
C SUBROUTINE SSS COMPUTES THE SURFACE SCATTERING STRENGTH OF      SSS 0200
C THE SURFACE WITH MEAN WAVE HEIGHT SIGMA AND MEAN SURFACE      SSS 0300
C SLOPE 1./CTS0BZ, BOTH FUNCTIONS OF WIND SPEED W IN KNOTS      SSS 0400
C
C
C DIMENSION TERM(100)          SSS 0500
C COMMON/SSS PRAM/W,PHISUB1,THETAR(3000),I      SSS 0600
C COMMON/SSS DATA/PHISURR,ANGRCUR,PLASS,RR,RDEP/H,FREQ,NOSOL,FLAG      SSS 0700
C *CO,SSUFS          SSS 0800
C SIGMA = .00092*w**(.5./2.)          SSS 0900
C CTS0BZ = 1./(.006 + .005202*w)          SSS 1000
C AVALEN = CO/(10J0,*FREQ)          SSS 1100
C PI = 3.1415926535          SSS 1200
C AVALNUM = 2.*PI/AVALEN          SSS 1300
C CON = PI/180.          SSS 1400
C THETAR(I) = I*THETAR(I)*CON          SSS 1500
C PHISURR = PHISURR*CON          SSS 1600
C CSPHI1 = COS(PHISUB1)          SSS 1700
C SNTHETAR = SIN(THETAR(I))          SSS 1800
C CSTHETAR = COS(THETAR(I))          SSS 1900
C SNPHI1 = SIN(PHISUB1)          SSS 2000
C SNPHIR = SIN(PHISURR)          SSS 2100
C CSPHIR = COS(PHISURR)          SSS 2200
C T = 2.*SIGMA*SQRTE(CTS0BZ)          SSS 2300
C AREA = 2500,          SSS 2400
C VSURXYSQ = AVALNUM**2*(CSPHI1**2 - 2.*CSPHI1*CSPHIR*CSTHETAR + CSPHISSS 2500
C *IR**2)          SSS 2600
C F = 1. + SNPHI1*SNPHIR - CSPHI1*CSPHIR*CSTHETAR          SSS 2700
C F = F/(SNPHI1*(SNPHI1 + SNPHIR))          SSS 2800
C VSUBX = (CSPHI1 - CSPHIR*CSTHETAR)*AVALNUM          SSS 2900
C VSUBY = -CSPHIR*SNTHETAR*AVALNUM          SSS 3000
C VSUBZ = WAVLLM*(SNPHI1 + SNPHIR)
C IF(VSUBX,EQ,0.0) RH01 = 1,          SSS 3200
C IF(VSUBY,EQ,0.0) GO TO 8          SSS 3300
C RH01 = SIN(50.*VSUBX)/(50.*VSUBX)
C IF(VSUBY,EQ,0.0) RH02 = 1.0          SSS 3400
C IF(VSUBY,EQ,0.0) GO TO 9          SSS 3500
C RH02 = SIN(50.*VSUBY)/(50.*VSUBY)
C RH0 = RH01*RH02          SSS 3600
C
C ROUGHNESS CRITERION IS DETERMINED          SSS 3700
C THIS IS ONLY FOR A ROUGH AND A MODERATELY ROUGH SEA SURFACE          SSS 3800
C
C G = VSURZ*VSUBZ*SIGMA*SIGMA          SSS 3900
C
C G MUCH GREATER THAN ONE CORRESPONDS TO A ROUGH SURFACE WHILE G          SSS 4000
C APPROXIMATELY EQUAL TO ONE CORRESPONDS TO A MODERATELY ROUGH          SSS 4100
C SURFACE.
C
C IF(G,LT,4.) GO TO 1          SSS 4200
C POWER = -1.+(VSURXYSQ*T*T/(4.*G))          SSS 4300
C RH0RH0ST = PI*F*F*T*T*EXP(-POWER)/(G*AREA)          SSS 4400
C GO TO 5          SSS 4500
C
C J = 1          SSS 4600
C A = PI*T*T*F*F*EXP(-G)          SSS 4700
C FACTOR = 1/J          SSS 4800

```

```

2 DENOM = FACTOR/J          SSS 4900
POWER = -1.*VSUBXY50*T*T/(4.*J)  SSS 5000
TERM(J) = G**J*EXP(-FACTOR)*DENOM  SSS 5100
IF(TERM(J).LE..0000001) GO TO 3  SSS 5200
J = J + 1                   SSS 5300
FACTOR = FACTOR/J            SSS 5400
IF(J = 100) 2, 2, 6          SSS 5500
3 SUM = 0                   SSS 5600
DO 4 N=1, J                 SSS 5700
SUM = SUM + TERM(N)         SSS 5800
4 CONTINUE                  SSS 5900
RHGRHST = A*SUM/AREA + EXP(-G)*RHA**2  SSS 6300
5 PRC = RHGRHST*SINPHI1**2*AREA/WAVLEN**2  SSS 6400
SSURS = 10.*ALOG10(PRC)        SSS 6500
RETURN                      SSS 6600
6 PRINT 7, TERM(100)         SSS 6700
7 FORMAT(* SERIES FOR SSURS FAILED TO CONVERGE RAPIDLY ENOUGH *, 1E11.4)
STOP                         SSS 6800
END

```

```

C SUBROUTINE DATA(RCRANGE,RANGE1,THETAR,INDEX1,RAN)
C DATA COMPUTES THE VALUES OF RCRANGE(I), THETAR(I), RANGE1(I), AND
C N, WHERE N IS THE TOTAL NUMBER OF SCATTERING POINTS TO BE CONSIDERED.
C
C DIMENSION RCRANGE(1),THETAR(1),T(4,8),RANGE1(1)
C I = 1
C DIST = 50
C RAND = RAN - DIST
C INDEX = 1
C INDEX1 = 0
C INDEX2 = 0
2 J = 1
RAN3 = RAN - RAND
TRAN = 0
C THIS COMPUTES RANGE1 USED BY ROUTINE THAT COMPUTES H (PROPAGATION
C LOSS OF ANY ONE RAY).
C
1 T(4,J) = SQRT(TRAN*TRAN + RAND*RAND)
INDEX2 = INDEX2 + 1
RANGE1(INDEX2) = T(4,J)
J = J + 1
TRAN = TRAN + DIST
IF (TRAN.LE.350) GO TO 1
J = 1
TRAN = 0
3 T(1,J) = SQRT(TRAN*TRAN + RAN3*RAN3)
C THIS PUTS RANGES IN PROPER ARRAY TO BE USED BY SURFSCAT
C
RCRANGE(INDEX) = T(1,J)
J = J + 1
TRAN = TRAN + DIST
INDEX = INDEX + 1
IF(TRAN.LE.350) GO TO 3
J = 1
TRAN = 0
4 T(2,J) = TRAN
TRAN = TRAN + DIST
J = J + 1
IF(TRAN.LE.350) GO TO 4
DO 6 J=1,8
THET1 = ATAN(T(2,J)/RAND)
THET2 = ATAN(T(2,J)/RAN3)
T(3,J) = 57.2958*(THET1 + THET2)
C THIS PUTS THETAR IN PROPER ARRAY TO BE USED BY SURFSCAT
C
INDEX1 = INDEX1 + 1
6 THETAR(INDEX1) = T(3,J)
I = I + 1
IF(I-9).EQ.10,10,10
9 RAND = RAND - DIST
IF(1000 - RAND).GT.2,2,112
10 I = 1
GO TO 9
112 CONTINUE
END

```

```

      SUBROUTINE COMPUTE H(RAN, HC, ZSUB0, WAVE, TEMP, SUMH, MX, H, GC) H 0100
C COMPUTE H COMPUTES THE SCATTERING LOSS FROM THE SOURCE TO A H 0200
C SCATTERING POINT (TL1), H AND SUMS THE EQUIVALENT INTENSITIES, H 0300
C 10**((H/10)). H 0400
C H 0500
C H 0600
C COMMON/SSSDATA/DUM1,DUM2,TL2,DUM3,DM,FREQ,DUM4,DUM5,CA,SSUBS H 0700
NR = RAN*SQRTE(GC)/SQRTE(8.*HC*CO)
QUAN = KR
IF(QUAN.LT.1.) QUAN = 1.
5 R = RAN/(1000.*SQRTE(3.*HC))
RAN = RAN/1000.
ZSUB0 = SQRTE(ZSUH0/HC)
ZEE = .3
ASUHS = 3.2*SQRTF(WAVE*FREQ)/SQRTE(3.*HC)
EXP = 6. - (2100./(TEMP + 459.6))
FSURT = 1.23*10.**EXP
ALPHA = .651*FSUBT*FREQ**2/(FREQ**2 + FSURT**2) + .0269*FREQ**2/FSH
*UBT
GOFZ = .1*10.**((2.3*(ZEE - ZSUB0))*(FREQ/25.)**(.1/3.))
F0FZEE = .4*10.**ZEE
F0FZSUB0 = .4*10.**ZSUB0
F0FZED = .4*10.**((ZEE - ZSUB0))
FACTOR = (FREQ/R.)**(.1/3.)
IF(FREQ.LE.8.) FACTOR = 1.
H0FZZ0 = (F0FZEE + F0FZSUB0 + F0FZED)*FACTOR
RSUB1 = (2. - ZEE - ZSUB0)/4.
IF(RAN.GE.RSUB1) GO TO 1
TL1 = 20.*ALOG10(RAN) + ALPHA*RAN + GOFZ*R/RSUB1 + 60.
GO TO 3
1 IF(R.GE.RSUB1 + .5) GO TO 2
TL1 = 20.*ALOG10(RAN) + ALPHA*RAN + 2.*(R - RSUB1)*H0FZZ0 + (1. - .52.*R - RSUB1)*GOFZ + 60.
GO TO 3
2 ARG1 = (RSUB1 + .5)*SQRTE(3.*HC)
TL1 = 10.*ALOG10(RAN) + RAN*(ALPHA + ASUHS) + H0FZZ0 - ASUHS*ARG1
1+ 10.*ALOG10(ARG1) + 60,
3 H = -TL1 - TL2 + SSUBS + 33.98 - QUAN*1.64*SQRTE(WAVE*FREQ*3.)
C H IS INCREMENTED BY 10*ALOG10(2) FOR SCATTERING POINTS OFF THE H 3900
C CENTER LINE TO ACCOUNT FOR THE PROPAGATION LOSS FROM THE SYMMETRIC H 4000
C SQUARE ON THE OPPOSITE SIDE OF THE CENTER LINE. H 4100
C H 4200
C H 4300
IF(MX,NF,1) H = H + 10*ALOG10(2.)
SUMH = SUMH + 10**((H/10))
RAN = 1000.*RAN
END

```

```

SUBROUTINE TABLE(MX) TAB 0100
C TABLE PRINTS OUT VALUES OF H, 10LOG(SSUBS), AND ANGRCVR IN TAB 0200
C TARULAR FORM. TAB 0300
C TAB 0400
C TAB 0500
C COMMON/SSS DATA/ANGSRCE,ANGRCVR,PLOSS,RR,RDEPTH,FREQ,NOSOL,FLAG, TAB 0600
100,SSUBS TAB 0700
COMMON/A/H TAB 0800
DIMENSION ARRAYH(8),ARRAYS(8),ARRAYA(8) TAB 0900
DATA(I = 100), (LINE = 21) TAB 1100
DATA(N = 0) TAB 1200
IF(I = 100)D , 7 TAB 1300
7 PRINT 30 TAB 1400
300FORMAT( 40X , 1HMM // 19X , 1H0 , 9X , 1H1 , 9X , 1H2 , 19X , 1H3 , 9X , 1H4 , 9X , 1H5 , 9X , 1H6 , 9X , 1H7 / 5X , 1HN / )TAB 1500
I = I + 100 TAB 1600
5 I = I + 1 TAB 1700
K = 1 TAB 1800
ARRAYH(I) = H TAB 1900
ARRAYS(I) = SSUBS TAB 2000
ARRAYA(I) = ANGRCVR TAB 2100
IF(I,EG,MX) GO TO 20 TAB 2200
10 RETURN TAB 2300
20 I = 0 TAB 2400
N = N + 1
IF(MX,EG,8,AND,ARRAYS(8).GE.,-60,) K = 0
M = MX - K
PRINT 40, (ARRAYH(J), J = 1, M)
PRINT 41, N, (ARRAYS(J), J = 1, M)
PRINT 42, (ARRAYA(J), J = 1, M)
LINE = LINE + 4
IF(LINE,GE,53) PRINT 44
IF(LINE,GE,53) LINE = 0
40 FORMAT(/, 13X, 3MH , 8(F8.2,2X)) TAB 2900
41 FORMAT(1X,15+3X,7HSSUBS ,8(F8.2,2X)) TAB 3000
42 FORMAT(7X, 9HANGRCVR , 8(F8.2, 2X)) TAB 3100
44 FORMAT(1H1)
END TAB 3200

```

```

SUBROUTINE AMOS          AM0 0100
C   AMOS COMPUTES ANOTHER VALUE FOR HT USING THE AMOS FORMULATIONS.  AM0 0200
C
COMMON/AN0Y/H, ZSUHC, ZEE, RAN, FREQ, WAVE, TEMP          AM0 0300
REAL LOSS1, LOSS2          AM0 0400
FREQ = 1000.*FREQ          AM0 0500
ALPHAS = 3.28*SORTF(WAVE*FREQ/(3000.*H))          AM0 0600
R = RAN/(SQRTF(3.*H)*1000.,)          AM0 0700
Z200 = ZSUHC          AM0 0800
ZSUHC = SORTF(ZSUHC/H)          AM0 0900
ZEN0 = ZEE          AM0 1000
ZEE = SQRTF(ZEE/H)          AM0 1100
ZED = ZEE - ZSUHC          AM0 1200
FREQ0 = (FREQ/25000.)**(1./3.)          AM0 1300
IF(ZED.GT.1.) GO TO 2          AM0 1400
GOFZED = (.1*10.**(.3*ZEN0))*FREQ0          AM0 1500
GO TO 3          AM0 1600
2 GOFZED = 20.*FREQ0          AM0 1700
3 FOFZED = .4*10.*ZED          AM0 1800
FOFZEE = .4*10.*ZEE          AM0 1900
FOFZ0 = .4*10.*ZSUHC          AM0 2000
HOFZ = FOFZED + FOFZEE + FOFZ0          AM0 2100
IF(FREQ.LT.8000.) GO TO 4          AM0 2200
HOFZ = HOFZ*(FREQ/8000.)**(1./3.)          AM0 2300
4 POWER = 6. - (2100./(TEMP + 459.6))          AM0 2400
FSUHT = 1.23*(10.*POWER)          AM0 2500
A = (.651*((FREQ/1000.)**2)*FSUHT/((FREQ/1000.)**2 + FSUHT**2)) + AM0 2600
*.0269*(FREQ/1000.)**2/FSURT          AM0 2700
IF(ZSUHC.GT.1.) GO TO 6          AM0 2800
IF(ZEE.GT.1.) GO TO 5          AM0 2900
RSUB1 = (ZEE - ZEE - ZSUHC)/4.          AM0 3000
GO TO 7          AM0 3100
5 RSUB1 = (1. - ZSUHC/4. + SORTF(ZEE**2 - 1.))/5.          AM0 3200
GO TO 7          AM0 3300
6 RSUB1 = (SQRIF(ZSUHC**2 - 1.) + SORTF(ZEE**2 - 1.))/5.          AM0 3400
7 VAL = AFSF(3.*ZEN0 - 3.*H)          AM0 3500
QUA = AFSF(3.*Z200 - 3.*H)          AM0 3600
TEST = 25. + SORTF(VAL) - SORTF(QUA) + 5.*RAN/1000.          AM0 3700
IF(TEST.LE.0.) TEST = 0.0          AM0 3800
LOSS2 = 20.*ALOG10(RAN) + A*(RAN/1000.) + TEST*FREQ0          AM0 3900
IF(R.GT.RSUB1) GO TO 10          AM0 4000
LOSS1 = 20.*ALOG10(RAN) + A*(RAN/1000.) + GOFZED*R/RSUB1          AM0 4100
IF(ZEE.LE.1..AND.ZSUHC.LE.1.) GO TO 8          AM0 4200
IF(LOSS1 - LOSS2) 8, 9, 9          AM0 4300
8 PLOSS = LOSS1          AM0 4400
GO TO 16          AM0 4500
9 PLOSS = LOSS2          AM0 4600
GO TO 16          AM0 4700
10 IF(R.GE.RSUB1+.5) GO TO 14          AM0 4800
PLOSS = 20.*ALOG10(RAN) + A*RAN/1000. + 2.*(R - RSUB1)*HOFZ +          AM0 4900
*(1. - 2.*(R - RSUB1))*GOFZED          AM0 5000
IF(ZSUB1.LE.1.) GO TO 16          AM0 5100
11 IF(PLOSS - LOSS2) 12, 13, 13          AM0 5200
12 GO TO 17          AM0 5300
13 PLOSS = LOSS2          AM0 5400
GO TO 14          AM0 5500
AM0 5600
AM0 5700

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```
14 PL0SS = 10.*AL0G10(RAN) + (A + ALPHAS)*RAN/1000. + H0F7 - ALPHAS AM0 5800
   **SQRTE(3.+H)*(RSUB1 + .5) + 10.*AL0G10(SQRTE(3.+H)*(RSUB1 + .5)) + AM0 5900
   *30,
   IF(7SUBR.GT.1.) GO TO 15
   GO TO 16
15 IF(PL0SS = LOSS2) 16, 17, 17
16 PL0SS = LOSS2
17 PL0SS = LOSS2
18 PRINT 90, PL0SS
90 FORMAT(5X*AM05 FORMULATIONS GIVE *,F5,1.* DR LOSS*)
      RETURN
      END
```

```

ENTRYIINITPTPP,PTCP ~ PTP00100
LIBRARY# RDPROFLE~ PTP00200
(I THIS COMMON BLOCK GIVES THESE TWO VALUES TO SUBROUTINE CMPUTE H) PTP00300
COMMONISNDSPDS(2);SURFACE VELOCITY,BOTTOM VELOCITY.~ PTP00400
COMMONSSSDATA(8);ANGSRCE,ANGRCVR,PLASS,RR,RDEPTH,FREQ,NOSOL,FLAG.~ PTP00500
COMMON#PROFILE(4012)~ PTP00600
MONTH,DAY,YEAR,LATITUDE,LONGITUDE, IDNO, PTP00700
ORIGINATOR(2), PTP00800
NR0FDEPTHs, BT,DONG,MTHD, PTP00900
DEPTH TABLEEXT(800), C*SOUNDSPEED TABLE(800), ASUBHNE#A1TABLE (800), PTP01000
ASUBTHW#A2TABLE(800), ASUBTHREE#A3TABLE(800).~, PTP01100
TX DEPTH# Z SUHTX = 000000.00000, PTP01200
RECEIVER DEPTH# RCVR DEPTH# ZSUBRC = 000000.00000, PTP01300
RECEIVER RANGE = 000000.0000, PTP01400
MODE,ANG, PTP01500
NR OF A1S# NMNR OF A1S, PTP01600
(#PAGE F5273-2) PTP01700
C OF SOURCE# TX SOUND SPEED = 0000.0000, PTP01800
MODE DIRECTION, PTP01900
MODE NUMBER = 00, PTP02000
RANGE# R(2)=0*0, PTP02100
DERIVATIVE# D(2)=0*0, PTP02200
RANGE SIGN # RS (2), PTP02300
DERIVATIVE SIGN# DS(2), PTP02400
EPSILON, PTP02500
DELTAV=0000.0000, PTP02600
CASE NUMBER# CN, PTP02700
VRR (6), PTP02800
VELOCITY# V(2)=0*0, PTP02900
V MAX# MAXIMUM VELOCITY, INITV, PTP03000
INITIAL VELOCITY=0000.0000, PTP03100
MAXVONPROFILE=0000.0000, MAXPROFILEDEPTH=0000.0000, 11, PTP03200
CMXZTAB (100), PTP03300
CMT# C MAX TABLE (100).~, PTP03400
MAIN PROGRAM DIMENSIONING.. PTP03500
INTERVAL SIZE=4.0 , PTP03600
ATTN FACTOR, FSQ,~ PTP03700
INITPTOP1=1.0ITXDEPTH, 1.0*37IRM, PTP03800
FLAG = 0 I RDPROFILE ~ ~ . PTP03900
97421.2034IVMAX, 1.0*-5IEPSILON, PROFILE LABEL, PTP04000
COMPUTE ATTN FACTOR, NR OF DEPTHS -1 I NR OF A1S, PTP04100
RDEPTHIRCVRDPFTH, PTP04200
SEARCH, NR0FA1S|BOTTOM INDEX, C|BOTTM INDEX|BOTTM VELOCITY, PTP04300
(MAXVONPROFILE-INITIALVELOCITY)/INTERVALSIZE|DELTAV, PTP04400
ADPR0INFO, PTP04500
C|TBII|TX SNDSPD|TX SOUNSPEED, CIRR1|RC SNDSPD, PTP04600
1|MODE, PTP04700
PTOP1=RRIREC1|VERANGE, NEWMODE, EXITPTOP1|NEXTTRC|NEXTMODE1, PTP04800
END OF RUNZ., PTP04900
LSTVINCLFLAG~, PTP05000
NEW MODEZ, PTP05100
+INITIAL VELFCITY + EPSILON + V + DELTA V + V[1], 1 + NOSOL, PTP05200
0|LSTVINCLFLAG, PTP05300
MODE < 0~, PTP05400
- 1 | MODE DIRECTION, $ MODE $ | MODE NUMBER~ (# UP) PTP05500
1 | MODE DIRECTION, MODE | MODE NUMBER~ (# DOWN) PTP05600
TRACE RAY (V, DM RANGE, DERIVATIVE, RANGE SIGN, DERIVATIVE SIGN), PTP05700

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DETERMINE CASEZ PTP05800
TRACE RAY (V[1], 0^ RANGE[1], DERIVATIVE [1], RANGE SIGN [1], DERIVATIVVPTP05900
E SIGN[1]), PTP06000
RAY TRACE MATRIX (RS, RS[1], DS, DS[1]^ CASE NUMBER), PTP06100
CASE SWITCH (CN), PTP06200
CASE SWITCH*, PTP06300
CASE 0, PTP06400
CASE 1, PTP06500
CASE 20, PTP06600
CASE 31, PTP06700
CASE 0^ NEXT INCREMENT, PTP06800
(*PAGE F5273-5) PTP06900
CASE 1Z PTP07000
CASE 1 FUNCTION (V, V[1], R, R[1], RS, RS[1]^ VRR, VRR[1]), PTP07100
TRACE SOLUTION RAYS (VRR, VRR[1]^), NEXT INCREMENT. PTP07200
CASE 20Z PTP07300
CASE 20 FUNCTION (V, V[1], R, R[1], RS, RS[1], DS, DS[1]^ PTP07400
VRR, VRR[1], VRR[2], VRR[3]), PTP07500
VRR = 0^ PTP07600
NEXT INCREMENT.^ PTP07700
TRACE SOLUTION RAYS (VRR, VRR[1]^), PTP07800
TRACE SOLUTION RAYS (VRR[2], VRR[3]^), NEXT INCREMENT, PTP07900
CASE 31Z PTP08000
CASE 31 FUNCTION (V, V[1], R, R[1], RS, RS[1], DS, DS[1]^ PTP08100
VRR, VRR[1], VRR[2], VRR[3], VRR[4], VRR[5]), PTP08200
TRACE SOLUTION RAYS (VRR, VRR[1]^), PTP08300
VRR [2] = 0^ PTP08400
NEXT INCREMENT.^ PTP08500
TRACE SOLUTION RAYS (VRR[2], VRR[3]^), PTP08600
TRACE SOLUTION RAYS (VRR[4], VRR[5]^), NEXT INCREMENT, PTP08700
(*PAGE F5273-6) PTP08800
NEXT INCREMENTZ PTP08900
V[1] | V + DFLTA V | V [1], RANGE [1] | RANGE, PTP09000
DERIVATIVE[1] | DERIVATIVE, RANGE SIGN [1] | RANGE SIGN, PTP09100
DERIVATIVE SIGN [1] | DERIVATIVE SIGN, PTP09200
V[1] < MAX V ON PROFILEZ PTP09300
DETERMINE CASE.^ PTP09400
LSTVINCFLAG=0^ PTP09500
1|LSTVINCFLAG, MAXVONPROFILE|V[1], PTP09600
DETERMINE CASE.^ PTP09700
LAST VINCREMNTZ PTP09800
TRACE RAY (VMAX, 0^ RANGE[1],, RANGE SIGN[1]), PTP09900
RANGE SIGN [1] = RANGE SIGNZ PTP10000
END OF MODE.^ PTP10100
CASE 1 FUNCTION (V, VMAX, R, R[1], RS, RS[1]^ VRR, VRR[1]), PTP10200
TRACE SOLUTION RAYS (VRR, VRR[1]^), PTP10300
END OF MODEZ,, PTP10400
AV=0000,000,Z PTP10500
TRACE SOLUTION RAYS (V (2), R (2), TT (2), SL (2), PTP10600
ATTN (2), PROP (2), ANGLE, DV (2) = 0*0, TSTEMP,)^ PTP10700
*TRACE RAY(V,1^R),TRACE RAY(V[1],1^R[1]), PTP10800
( RECEIVER RANGE - R ) / ( R [1] - R ) | TSTEMP, PTP10900
INTERP (TS TFP, V, V [1]^ V), PTP11000
TRACE RAY (V, 1^ R, DV,,, TT, SL, ATTN), PTP11100
FIND ANGLE (VA ANGLE), ATTN + SL | PROP, PTP11200
0 | NOSL, PTP11300
ANGLE|ANGSRCE,PROP|PLLOSS,EXITPTOP, PTP11400

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```

FIND ANGLE (V, ANG.)*
- TX SOUND SPEED / V | ANG, ARCCOS (ANGA ANG),
ANG = 57.2957795 | ANG*
INTERP (RATIO, X (2), VAL)* -> RATIO * (X (1) - X) + X | VAL* ..
DD=00,MM=00,YY=0000,LONG=000.00,LAT=000.00, ID={1}, BTNO=000,
ORIG(2) = {XXXXXXXX},
DONC BUFF=000000,
MTHD BUFF=00,
FREQUENCY = 00000.000,^
PROFILE LABEL#*
DAY|DD,MONTH|MM,YEAR|YY,LONGITUDE|LONG,LATITUDE|LAT, IDNO|ID,
BTB|BTNO, ORIGINATOR|ORIG,
ORIGINATOR|1| ORIG|1|,
DONC|DONCBUFF, MTHD | MTHDRBUFF,
+>PRINTER<>^ << POINTS TO POINTS RAYS TRACING >>,
<< PROFILES INFORMATION >>,
<<?DATE>|MM|DD|YY>
<<?LATITUDE>|LAT>
<<?LONGITUDE>|LONG>
<<?IDSNO,>|ID>
<<ORIGINATOR>|$ORIG|$ORIG|1>*+
ADPROINFO**+
*><<MAX$VS$ON$PROFILE>>MAXV$ONPROFILE>
<<DEPTH$OF$MAX$VS$ON$PROFILE>>MAXPROFILEDEPTH>
<<INITIAL$VEI$CITY>>INITIALVELOCITY>
<<DELTA$VELOCITY>>DELTAV>
<<INTERVAL$SIZE>>INTERVALSIZE>*+
COMPUTE ATTN FACTOR*
+FREQ * FREQ | FSG * 0.04 / (4100.0 * FSG) + 2.75 * -7 * FSG
| ATTN FACTOR*.
7
(*PAGE F5494+1)
RANGE MAXIMUM# RM,
PATH LENGTH,
MODE COUNT,
COS THETA SUB0, TAN THETA SUB0,
TEMP (5),
UP OR DOWN, HI, LO,
LBI, UBI,          (FLWFR AND UPPER BOUNDARY INDICES)
VERTEX FLAG,
ZR FLAG,
BOUNCE FLAG,
ZR1STINC FLAG,
APEX, NADIR,
ABI, NRI,          (APEX AND NADIR BOUNDARY INDICES)
BOTTOM INDEX, SURFACE INDEX,
HALF CYCLE FLAG,
RANGE TABLE (100),
TRAVEL TIME TABLE (100),
DERIVATIVE TABLE (100),
PATH LENGTH TABLE (100).^
(*PAGE F5494+2)
TRACE RAY (V, SOLUTION FLAG, RANGE, DERIVATIVE,
RANGE SIGN, DERIVATIVE SIGN, TRAVELTIME, SPRD LOSS, ATTENUATION.)*
+0 | RANGE | DERIVATIVE | MODE COUNT | HALF CYCLE FLAG | APEX | NADIR | NRI
| VERTEX FLAG | BOUNCE FLAG | ZRFLAG | ZR1STINC FLAG,
PTP11500
PTP11600
PTP11700
PTP11800
PTP11900
PTP12000
PTP12100
PTP12200
PTP12300
PTP12400
PTP12500
PTP12600
PTP12700
PTP12800
PTP12900
PTP13000
PTP13100
PTP13200
PTP13300
PTP13400
PTP13500
PTP13600
PTP13700
PTP13800
PTP13900
PTP14000
PTP14100
PTP14200
PTP14300
PTP14400
PTP14500
PTP14600
PTP14700
PTP14800
PTP14900
PTP15000
PTP15100
PTP15200
PTP15300
PTP15400
PTP15500
PTP15600
PTP15700
PTP15800
PTP15900
PTP16000
PTP16100
PTP16200
PTP16300
PTP16400
PTP16500
PTP16600
PTP16700
PTP16800
PTP16900
PTP17000
PTP17100

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I TRAVEL TIME | SURFACE INDEX | PATH LENGTH, -1 | ABI,          PTP17200
V = TX SOUND SPEED#                                PTP17300
FIND DIRECTION#
  V > CMT [TBI - 1]#                                PTP17400
  V < CMT [TBI + 1]#                                PTP17500
    - 1 | MODE DIRECTIONAL ERROR INC.^ (ZADIR)      PTP17600
  V > CMT [TBI+1]#                                PTP17700
    1 | MODE DIRECTIONAL ERROR INC.^ (ZAPEX)        PTP17800
  1 | ZR FLAG | ZR1STINC FLAG, 1.0 | COSTHETA SUB0,   PTP17900
  0 | TANTHETA SUB0, CONT.^                         PTP18000
C OF SOURCE / V | COS THETA SUB0, 1.0 / COS THETA SUB0 | TEMP * PTP18200
TEMP - 1.0 | TEMP [1], SQRT (TEMP [1]^ TAN THETA SUB0), PTP18300
CONT#
MODE DIRECTION | UP OR DOWN = 1#      (*1, E, DOWN) PTP18400
TBI = BOTTOM INDEX#                                PTP18500
  -UP OR DOWN | UP OR DOWN, UP, DOWN.^              PTP18600
TBI = 0#                                           PTP18700
  -UP OR DOWN | UP OR DOWN, DOWN, UP.^              PTP18800
DOWN# TBI | LBI | LO | HI + 1 | URI, CONT1,
  URI TBI | URI | LO | HI - 1 | LBI,                PTP18900
CONT1#
ZR1STINC FLAG (* 0 - UP OR DOWN | UP OR DOWN)^     PTP19000
(*PAGE F5494-3)                                     PTP19100
NEXT LAYER#
UP OR DOWN = 1#
  LBI = RBI#
    INCREASE MODE COUNT.^                         PTP19200
  URI = RBI#
    INCREASE MODE COUNT.^                         PTP19300
PTP19400
CONTINUE TRACING,
INCREASE MODE COUNT#                                PTP19500
MODE COUNT + 1 | MODE COUNT ≥ MODE NUMBER#        PTP19600
SET SIGNS.^                                         PTP19700
CONTINUE TRACING#
HALF CYCLE FLAG (* 0#
  BRIC.^                                         PTP19800
  LBI ≥ LO | UHI ≤ HI#                           PTP19900
  BRIC.^                                         PTP20000
SOLUTION FLAG = 1#                                 PTP20100
COMPUTE RANGE (V, LBI, SOLUTION FLAG),
RANGE TABLE (LBI), DERIVATIVE TABLE (LBI),           PTP20200
TRAVEL TIME TABLE (LBI), PATH LENGTH TABLE (LBI),   PTP20300
COMPUTE RANGE (V, LBI, 0^ RANGE TABLE (LBI),         PTP20400
DERIVATIVE TABLE (LBI),,, VERTEX FLAG)^            PTP20500
(*PAGE F5494-4)
ZR1ST INC FLAG (* 0#
  0 | ZR1STINC FLAG,                                PTP20600
  MODE DIRECTION = 1#                                PTP20700
    HI + 1 | HI | LO^                            PTP20800
    HI - 1 | HI | LO^                            PTP20900
  BRIC.^                                         PTP21000
  UP OR DOWN = 1#                                 PTP21100
    HI + 1 | HI^                                PTP21200
    LO - 1 | LO^                                PTP21300
  VERTEX FLAG = 0#                                PTP21400
    BRIC.^                                         PTP21500
  UP OR DOWN = 1#      (*VERTEXED)               PTP21600
PTP21700
PTP21800
PTP21900
PTP22000
PTP22100
PTP22200
PTP22300
PTP22400
PTP22500
PTP22600
PTP22700
PTP22800

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```

1 | NADIR, LBI | NBI ≤ RBI*
SOLUTION FLAG(0X RCVR OUTSIDE.^
    NEXT INCREMENT.^
1 | APEX, LBI | ABI > RBI*
SOLUTION FLAG(0X RCVR OUTSIDE.^
    NEXT INCREMENT.^
CONT VERTEX*
APEX = NADIR ? BOUNCE FLAG = 1^
    1 | HALF CYCLE FLAG.^
0 | VERTEX FLAG.
BYPASS RANGE INCREMENT COMPUTATION^ BRICK^
RANGE + RANGE TABLE (LBI) | RANGE > RANGE MAXIMUM^
    NEXT INCREMENT.^
ZR FLAG ( 0X
    ATT.^
SOLUTION FLAG ( 0X
    PATH LENGTH + PATH LENGTH TABLE (LBI) | PATH LENGTH^
DERIVATIVE TABLE (LBI) + DERIVATIVE | DERIVATIVE,
ATT^ TRAVEL TIME + TRAVEL TIME TABLE (LBI) | TRAVEL TIME,
(*PAGE F 5494-5)
UBI = NBI ? LBI = ABI^
    MCAVTX, (*RAY HAS VERTEXED)
UBI ≥ BOTTOM INDEX^
    APEX = 1^
        1 | HALF CYCLEFLAG.^ 1 | BOUNCE FLAG, RHB,
LBI ≤ SURFACE INDEX^
    NADIR = 1^
        1 | HALF CYCLE FLAG.^ 1 | BOUNCE FLAG, RHB, NBDRV,^
RHB^
    (*RAY HAS BOUNCED)
RANGE TABLE (LBI) + RANGE | RANGE,
DERIVATIVE TABLE (LBI) + DERIVATIVE | DERIVATIVE,
SOLUTION FLAG ( 0X
    TRAVEL TIME + TRAVEL TIME TABLE (LBI) | TRAVEL TIME,
    PATH LENGTH + PATH LENGTH TABLE (LBI) | PATH LENGTH.^
(*MODE COUNT MAY NEED TO BE INCREASED IF RAY HAS VERTEXED OR BOUNCED AT PTP26400
    THE RECEIVER DEPTH NECESSITATING THIS DOUBLE CHECK WHICH IS DONE PTP26500
    AT THE ENTRY POINT **NEXT LAYER**)
    MCAVTX^MODE CHECK AT VERTEX*
    *UPORDOWN|UPORDWN=1^
        LBI(RBI)NBDRV.^
        UBI(RBI)NBDRV.^
    MODE COUNT+1|MODE COUNT>MODE NUMBER^
        SET SIGNS.^
    NO BOUNCE OR VERTEX^ NBDRV^
    (*PAGE F5494-6)
    UP OR DOWN = 1^
        LBI | LBI + 1 | UBI^
        LBI | UBI - 1 | LBI^
    NEXT LAYER,
    SET SIGNS^
    ZR FLAG ( 0X
        0 | ZRFLAG,
        TRACE RAY EXIT.^
    RANGE ≥ RECEIVER RANGE^
        1 | RANGE SIGN^
        -1 | RANGE SIGN.^

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PTP22900
 PTP23000
 PTP23100
 PTP23200
 PTP23300
 PTP23400
 PTP23500
 PTP23600
 PTP23700
 PTP23800
 PTP23900
 PTP24000
 PTP24100
 PTP24200
 PTP24300
 PTP24400
 PTP24500
 PTP24600
 PTP24700
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 PTP25000
 PTP25100
 PTP25200
 PTP25300
 PTP25400
 PTP25500
 PTP25600
 PTP25700
 PTP25800
 PTP25900
 PTP26000
 PTP26100
 PTP26200
 PTP26300
 PTP26400
 PTP26500
 PTP26600
 PTP26700
 PTP26800
 PTP26900
 PTP27000
 PTP27100
 PTP27200
 PTP27300
 PTP27400
 PTP27500
 PTP27600
 PTP27700
 PTP27800
 PTP27900
 PTP28000
 PTP28100
 PTP28200
 PTP28300
 PTP28400
 PTP28500

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DERIVATIVE ≥ 0#
  1 | DERIVATIVE SIGN#
  -1 | DERIVATIVE SIGN#
SOLUTION FLAG = 0#^
COMPUTE SPREADING LOSS#
UP OR DOWN ( 1#
!COMMENT# THESE ALTERNATIVES ARE REVERSED WHEN COMPARED TO THE ONES
IN THE RAY TRACE PROGRAM. THIS IS DUE TO THE FACT THAT THE
UBI AND UBI HAVE ALREADY BEEN INCREMENTED (DECREMENTED) PRIOR TO
THE MODE COUNT CHECK.#
  C (UBI) / V | TEMP#
  C(LAI)/VTEMP#
ARCCOS(TEMP*ANGRCVR) , ANGRCVR=57,29577951ANGRCVR,
TEMP=1.0#
TRACE RAY EXIT.#
1.0 - TEMP * TEMP | TEMP, SQRT (TEMP^ TEMP),
$RANGE + DERIVATIVE + TEMP/COSTHETA SUB 0$ | TEMP,
LOG (TEMP* TEMP), 10.0 * TEMP | SPRD LOSS,
COMPUTE ATTENUATION#
ATTN FACTOR + PATH LENGTH | ATTENUATION#
TRACE RAY EXIT.#
(*PAGE F5494-7)
ERROR INC#, ->PRINTER <>n <<YOU HAVE CHOSEN A RELATIVE#
MAXIMUM$OF$MINIMUM$ON$THE$PROFILE>> <<AS YOUR#
VERTEX$VELOCITY,>>#
TRACE RAY EXIT.#
RCVR OUTSIDE#
(*IT IS POSSIBLE THAT THE RAY COULD HAVE VERTEXED AT THE RECEIVER LAYER#
AND THEREFORE IT SHOULD BE CHECKED BEFORE SAYING THE RECEIVER IS#
OUTSIDE THE RAY PATH.)#
UPORDOWN=1#
  $Z(1)+RCVR DEPTH$<0.1#
    CONT VERTEX.##
  $Z-RCVR DEPTH$<0.1#
    CONT VERTEX.##
    ->PRINTER<<THE RECEIVER IS LOCATED EITHER ABOVE OR#
BELOW THE RAY PATH>>#
TRACE RAY EXIT#,,#
RCK(4),#
RKEY,#
Z (2).#
A1, A2, A3,#
VSO,#
ALPHA, BETA (2),#
RENO,#
TANTHETA (2),#
BETATS.#
R00T1 = 0*0, R00T2 = 0*0,#
CMAXIN LAYER.#
(*THIS FLOWCHART CONTAINS COMPUTE RANGE FUNCTIONS#
WHICH COMPUTE RANGE, DERIVATIVE AND TRAVEL TIME)#
(*PAGE F5494-8)
COMPUTE RANGE (V SUBX, TABLE INDEX#TI, SF, RSUBI, DSUBI, TSUBI, PL SUBI)#
  . VF)#
-DEPTH TABLE (TI) | Z, DEPTH TABLE (TI+1) | Z(1),#
A1TABLE (TI) | A1, A2 TABLE (TI) | A2, A3 TABLE (TI) | A3,#
FIND ALPHA#
```

PTP28600
PTP28700
PTP28800
PTP28900
PTP29000
PTP29100
PTP29200
PTP29300
PTP29400
PTP29500
PTP29600
PTP29700
PTP29800
PTP29900
PTP30000
PTP30100
PTP30200
PTP30300
PTP30400
PTP30500
PTP30600
PTP30700
PTP30800
PTP30900
PTP31000
PTP31100
PTP31200
PTP31300
PTP31400
PTP31500
PTP31600
PTP31700
PTP31800
PTP31900
PTP32000
PTP32100
PTP32200
PTP32300
PTP32400
PTP32500
PTP32600
PTP32700
PTP32800
PTP32900
PTP33000
PTP33100
PTP33200
PTP33300
PTP33400
PTP33500
PTP33600
PTP33700
PTP33800
PTP33900
PTP34000
PTP34100
PTP34200

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4.0 * A1 + TEMP, A2 + A2 + TEMP[1],
V SUBX * V SUBX + VSQ * A3 + TEMP[2],
TEMP + (TEMP[2] + 1.0) - VSQ + TEMP[1] + ALPHA,
(*THE FOLLOWING 4 LINES CHECK FOR VERTEXING BETWEEN LAYERS)
A1 < 0*
    VT1* VSUBX > C[TI+1] + VSUBX > C[TI]*
        NO VERTEX IN LAYER.
        VERTEX IN LAYER.
    -A2/(2.0 + A1) + TEMP[3].
Z < TEMP[3] < Z[1]* VT1.
C MAX TABLE (TII) + C MAX IN LAYER ≥ V SUBX*
    VERTEX IN LAYER ≠ 1 + VF*
        NO VERTEX IN LAYER ≠ 0 + VF**
(*PAGE F5494-9)
(*THE FOLLOWING 13 LINES DETERMINE WHICH RANGE EQUATION
SHOULD BE USED)
VF = 0*
    A1 > 0*
        1 + REN0*
            2 + REN0**
        A1 > 0*
            UP OR DOWN = 1*
                3 + REN0*
                    6 + REN0**
            UP OR DOWN = 1*
                5 + REN0*
                    4 + REN0**
(*PAGE F5494-10)
RANGESWIX
FIND BETAS*
2.0 * A1 + TEMP[4] * Z + A2 + BETA,
TEMP[4] * Z[1] + A2 + BETA[1],
RANGE SWITCH (REN0-1),
RANGE SWITCH*
RANGE EQUATION 1,
RANGE EQUATION 2,
RANGE EQUATION 3,
RANGE EQUATION 4,
RANGE EQUATION 5,
RANGE EQUATION 3A,
(*PAGE F5494-11)
RANGE EQUATION 1*
RANGE FUNCTION 1(V SUBX, BETA, BETA[1], ALPHA+ RSUBI), CD,
RANGE EQUATION 2*
RANGE FUNCTION 2(VSUBX, BETA, BETA[1], ALPHA+ RSUBI), CD,
RANGE EQUATION 3*
RANGE FUNCTION 3(VSUBX, BETA, ALPHA+ RSURI), CD,
RANGE EQUATION 4*
RANGE FUNCTION 4(VSUHX, BETA[1], ALPHA+ RSURI), CD,
RANGE EQUATION 5*
RANGE FUNCTION 5(VSUBX, BETA, ALPHA+ RSUBI), CD,
RANGE EQUATION 3A*
RANGE FUNCTION 3(VSUBX, BETA[1], ALPHA+ RSUBI),
(*PAGE F5494-12)
COMPUTE DERIVATIVE* CDX
VF = 1*
    UP OR DOWN = 1*

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PTP34300
PTP34400
PTP34500
PTP34600
PTP34700
PTP34800
PTP34900
PTP35000
PTP35100
PTP35200
PTP35300
PTP35400
PTP35500
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PTP39400
PTP39500
PTP39600
PTP39700
PTP39800
PTP39900

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TAN THETA FUNCTION (Z^ TAN THETA), BETA | BETA TSA          PTP40000
TAN THETA FUNCTION (Z (1)^ TAN THETA), BETA (1) | BETA TSA    PTP40100
ZR FLAG ( 0#                                         PTP40200
COMPUTE TRAVEL TIME.^                                PTP40300
$TAN THETA SUB0 * (RSUBI + 4.0 * BETA TS / (ALPHA * TAN THETA))$ | DSUBPTP40400
!^                                         PTP40500
TAN THETA FUNCTION (Z^ TAN THETA), PTP40600
TANTHETA=0#                                         PTP40700
, <<TAN$THETA$ZERO.,>> DVB2#                         PTP40800
TAN THETA FUNCTION (Z(1)^ TAN THETA(1)), PTP40900
ZR FLAG ( 0#                                         PTP41000
COMPUTE TRAVEL TIME.^                                PTP41100
-$TAN THETA SUB0 * (RSUBI + (2.0/ALPHA) * PTP41200
(BETA(1)/TAN THETA (1) - BETA/TAN THETA)) $ | DSUBI# PTP41300
SF * 0# EXIT COMPUTE RANGE.^                        PTP41400
(# TRAVEL TIME COMPUTED SINCE THIS IS A SOLUTION RAY) PTP41500
COMPUTE TRAVEL TIME#                                PTP41600
0.25/(A1 * VSUBX) | TEMP, ALPHA + 8.0*A1 | TEMP (1), PTP41700
2.0 * BETATS * TAN THETA | TEMP (2),                PTP41800
VF = 1#                                         PTP41900
UP OR DOWN = 1#                                     PTP42000
- TEMP (2) | TEMP (2)##                           PTP42100
TEMP * (TEMP (2) + 0.5 * TEMP (1) * RSUBI) | TSUBI# PTP42200
TEMP * (BETA(1) * TAN THETA (1) - BETA * TAN THETA + PTP42300
0.5 * TEMP (1) * RSUBI) | TSUBI#                  PTP42400
(*PAGE F 5494-13)                                    PTP42500
FIND PATH LENGTH#                                 PTP42600
ZR FLAG ( 0#                                         PTP42700
EXIT COMPUTE RANGE.^                                PTP42800
VF = 1#                                         PTP42900
Z (1) - Z | PLSUBI * PLSUBI + RSUBI * RSUBI | PLSUBI, PTP43000
SQRT (PLSUBI*PLSUBI), EXIT COMPUTE RANGE.          PTP43100
FIND VERTEXING DEPTH# FVD#                         PTP43200
SOLVE QUAD IN Z (V SUBX, A1, A2, A3^ RROOT1, RROOT2), PTP43300
Z ≤ RROOT1 ≤ Z (1) #                               (*COMPARISON v1) PTP43400
Z ≤ RROOT 2 ≤ Z (1) #                            PTP43500
UP OR DOWN { 1#                                     PTP43600
RROOT 1 > RROOT 2#                                PTP43700
RROOT 2 | Z#                                         PTP43800
RROOT 1 | Z##                                       PTP43900
RROOT 1 > RROOT 2#                                PTP44000
RROOT 1 | Z (1)##                                  PTP44100
RROOT 2 | Z (1)##                                  PTP44200
UP OR DOWN { 1#                                     PTP44300
RROOT 1 | Z#                                         PTP44400
RROOT 1 | Z (1)##                                  PTP44500
(*PAGE F 5494-14)                                    PTP44600
Z ≤ RROOT 2 ≤ Z (1) #                             (*BEGIN FALSE v1) PTP44700
UP OR DOWN { 1#                                     PTP44800
RROOT 2 | Z#                                         PTP44900
RROOT 2 | Z (1)##                                  PTP45000
DHEC CK RROOT.^                                   PTP45100
FPL# Z (1) - Z | PLSUBI * PLSUBI + (RSUBI * RSUBI) / 4.0 | PLSUBI, PTP45200
SQRT (PLSUBI*PLSUBI), 2.0 * PLSUBI | PLSUBI, PTP45300
EXIT COMPUTE RANGE.                                PTP45400
ROOT ERROR#                                         PTP45500
, << ERROR $ IN $ PATH $ LENGTH $ COMPUTATION >> PTP45600

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<< BOTH $ ROOTS 1 OF $ QUADRATIC $ ARE $ OUTSIDE $ LAYER >>          PTP45700
<< ROOT 1$ => ROOT 1>>,NEXT MODE.
<<ROOT2$=>ROOT2>>,NEXT MODE.
DBLE CK ROOT2#
SZ-ROOT1$|RCK,
SZ-ROOT2$|RCK[1],
SZ[1]-ROOT1$|RCK[2],
SZ[1]-ROOT2$|RCK[3],
RCK<RCK[1]#
    RCK<RCK[2]#
        RCK<RCK[3]#
            0|RKEYn
            3|RKEYn
            RCK[2]<RCK[3]#
                2|RKEYn
                3|RKEYn
            RCK[1]<RCK[2]#
                RCK[1]<RCK[3]#
                    1|RKEYn
                    3|RKEYn
            RCK[2]<RCK[3]#
                2|RKEYn
                3|RKEYn
RCK[RKEY]<0,1#n
    ROOT ERROR.
SETVN[RKEY],          PTP48000
SETVN#          PTP48100
SETRCK,          PTP48200
SETRCK1,          PTP48300
SETRCK2,          PTP48400
SETRCK3,          PTP48500
SETRCK# ROOT1|Z,FPL.          PTP48600
SETRCK1#ROOT2|Z,FPL.          PTP48700
SETRCK2#ROOT1|Z[1],FPL,          PTP48800
SETRCK3#ROOT2|Z[1],FPL,          PTP48900
EXIT COMPUTE RANGE#          PTP49000
ZR1STINC FLAG (0#          PTP49100
    0 | VF, -IP OK DOWN | UP OR DOWN,          PTP49200
    RSURI / 2.0 | RSURI, TSURI / 2.0 | TSUBInn
(*PAGE F 5494-15)          PTP49300
SOLVE QUAD IN Z (VQ = 0*0, A1Q = 0*0, A2Q = 0*0, A3Q = 0*0, R1, R2, TS          PTP49400
(4),)*          PTP49500
+VQ * VQ | TS * TS | TS (1),
4.0 * TS * A1Q * (TS * A3Q - 1.0) | TS (2),
TS (1) * A2Q * A2Q - TS (2) | TS (3) < 0#          PTP49600
    DISC ERROR,^          PTP49700
SQRT (TS (3)^ TS (3)),          PTP49800
+(TS * A2Q - TS (3)) / (2.0 * TS * A1Q) | R1,
+(TS * A2Q + TS (3)) / (2.0 * TS * A1Q) | R2, SQFX.          PTP49900
DISC ERROR#, <>n << ERROR $ IN $ PATH $ LENGTH $ COMPUTATION >>
<< V $ => Vn ><< A1 $ => A10> << A2 $ => A20> << A3$ => A30>#
,NEXT MODE,
SQEX#;
TAN THETA FUNCTION (DZ, TITS,)*
+VSG *(A1 * DZ * DZ + A2 * DZ * A3) - 1.0 | TITS,
SQRT (TTTS^ TITS)*..
7

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(*PAGE F5494-16)
VB(2),
VB SQ(2),
RE TEMP(B),
PI OVER TWO = 1.5707963268
RANGE FUNCTION$#
RANGE FUNCTION 1(VEE, B(2), ALF, R.)#
-VEE * B | VB * VB | VB SQ + ALF | RETEMP,
VEE = B[1] | VH[1] * VH[1] | VH SQ[1] + ALF | RETEMP [1],
SQRT (RE TEMP^ RF TEMP), SORT (RE TEMP[1]^ RF TEMP[1]),
(VB[1] + RE TEMP[1])/(VB + RE TEMP) | RE TEMP [2],
LN (RETEMP[2]^ RETEMP[3]),
VEE = VEE * A1 | RE TEMP[4], SQRT (RETEMP[4]^ RETEMP[4]),
1.0 / RE TEMP[4] * RE TEMP[3] | R,
RANGE FUNCTION 2(VEE, B(2), ALF, R.)#
-SORT (-ALF^ RETEMP),
VEE = B/RETEMP | RETEMP[1], VEE = B[1]/RETEMP | RETEMP[3],
- VEE * VEE * A1 | RETEMP[5], SQRT (RETEMP[5]^ RETEMP[6]),
RETEMP[1]<1.0#
VERTEX IN LAYER,
RETEMP[3]<1.0#
VERTEX IN LAYER,
ARC SIN (RETEMP[1]^ RETEMP[2]), ARCSIN (RETEMP[3]^ RETEMP[4]),
(RETEMP[2] - RETEMP[4])/RETEMP[6] | R#
(*PAGE F5494-17)
RANGE FUNCTION 3(VEE, B, ALF, R.)#
-VEE * B | VB * VB | VB SQ + ALF | RE TEMP, $VB$ | VB, $ ALF$ | RETEMP
[6],
SQRT (RETEMP^ RETEMP[1]), SQRT (RETEMP [6]^ RETEMP [2]),
(VB + RETEMP[1])/RETEMP[2] | RETEMP[3],
LN (RETEMP[3]^ RETEMP[4]), VEE * VEE * A1 | RETEMP[5],
SQRT (RETEMP[5]^ RETEMP[6]),
2.0/RETEMP[6] * RETEMP[4] | R,
RANGE FUNCTION 4(VEE, B, ALF, R.)#
-VEE * VEE * A1 | RETEMP, SQRT (-RETEMP^ RETEMP[1]),
SORT (-ALF^ RETEMP[2]), VEE * B/RETEMP[2] | RETEMP[3],
ARC SIN (RETEMP[3]^ RETEMP[4]),
(PI OVER TWO * RETEMP[4]) * 2.0/RETEMP[1] | R#
(*PAGE F5494-18)
RANGE FUNCTION 5(VEE, B, ALF, R.)#
-VEE * VEE * A1 | RETEMP, SQRT (-RETEMP^ RETEMP[1]),
SORT (-ALF^ RETEMP[2]), VEE * B/RETEMP[2] | RETEMP[3],
ARCSIN (RETEMP[3]^ RETEMP[4]),
(RETEMP[4] + PI OVER TWO) * 2.0/ RETEMP[1] | R,
ERR IN ARC2#
,<<<ERROR$IN$RANGE$EQUATION2,$*ARCSIN$ARG$GT.$1,0>>..,
7#
(*PAGE F5494-19)
RAY TRACE MATRIX (RSIGN(2), D SIGN(2)^ CASE NUMBER, ROW, COLUMN, EN,
CASE TABLE (16)= 2, 2, 3, 1, 0, 2, 1, 1, 1, 2, 0, 1, 3, 2, 2)*
#0 | ROW | COLUMN,
RSIGN = 1#
2 | ROW#
D SIGN = 1#
ROW + 1 | ROW#
R SIGN (1) = 1#
2 | COLUMN#
PTP51400
PTP51500
PTP51600
PTP51700
PTP51800
PTP51900
PTP52000
PTP52100
PTP52200
PTP52300
PTP52400
PTP52500
PTP52600
PTP52700
PTP52800
PTP52900
PTP53000
PTP53100
PTP53200
PTP53300
PTP53400
PTP53500
PTP53600
PTP53700
PTP53800
PTP53900
PTP54000
PTP54100
PTP54200
PTP54300
PTP54400
PTP54500
PTP54600
PTP54700
PTP54800
PTP54900
PTP55000
PTP55100
PTP55200
PTP55300
PTP55400
PTP55500
PTP55600
PTP55700
PTP55800
PTP55900
PTP56000
PTP56100
PTP56200
PTP56300
PTP56400
PTP56500
PTP56600
PTP56700
PTP56800
PTP56900
PTP57000

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D SIGN (1) = 1#*
    COLUMN +1 I COLUMNS
4 * COLUMN + ROW I EN, CASE TABLE (EN) I CASE NUMBER*,.
7
(*RAY ACOUSTIC - CASE FUNCTIONS)
(*PAGE F5276-1)
(*THIS FLOWCHART CONTAINS THE FUNCTIONS USED TO DETERMINE THE
VERTEX VELOCITIES BETWEEN V AND V(1) FOR WHICH A RAY WILL STRIKE THE REPTP57100
RECEIVER)
RTOLERANCE = 100.0,
V TOLERANCE = 1.0 * -2#
CASE FUNCTIONS*
CASE 1 FUNCTION (V (2) = 0*0, R (2) = 0*0, RSIGN (2), VP = 0*0, V2P = 0PTP57200
*0,
RP = 0*0, R2P = 0*0, RP SIGN, R2 PSIGN)*#
FIND SOLUTION*
(*A LINEAR INTERPOLATION METHOD IS USED TO FIND SOLUTION)
INTERSECT PT (V, R, V (1), R (1)* VP), TRACE RAY (VP, 0* RP,, RPSIGN),
RP SIGN = R SIGN#
    INTERSECT PT (V, R, VP, RP* V2P), VP I V, RP I R#
    INTERSECT PT (VP, RP, V (1), R (1)* V2P), VP I V (1), RP I R (1)*
V < V2P < V (1)*
    CIR# (V (1) + V) / 2.0 I V2P#
TRACE RAY (V2P, 0* R2P,, R2PSIGN),
R2PSIGN = RSIGN#
    V2P I V, R2P I R#
    V2P I V (1), R2P I R (1)*
(*PAGE F 5276-2)
TEST#
V (1) - V $ V TOLERANCE# NOW TEST RANGES.^
$ 1.0 = RECEIVER RANGE / R $ < V TOLERANCE ?
$ 1.0 = RECEIVER RANGE / R (1) $ < V TOLERANCE#
CIR,
    FIND SOLUTION,
NOW TEST RANGES#
$ RECEIVER RANGE-R$ < R TOLERANCE !
$ RECEIVER RANGE - R (1) $ < R TOLERANCE#
V (1) - V < 1.0 * -5#
    CASE1 EXIT,
    CIR,^
CASE 1 EXIT#
V I VP, V (1) I V2P#
INTERSECT PT (V, R, V1, R1, V INTERSECT)*
*(RECEIVER RANGE - R) * (V1 - V) / (R1 - R) + V I V INTERSECT,* PTP60000
(*PAGE F 5276-3)
CASE 20 FUNCTION (V (2), R (2), RSIGN (2), DSIGN (2), VRR (4), RR (4),
    RP, RPSIGN, DP, DPSIGN, VP, PP20, ORIGVP,)* PTP60100
*RECYCLE 20#
2.0 I PP20,
V (1) - V < 1.0*-2#
    0 I VRR I VRR (1) I VRK (2) I VRR (3), CASE 20 EXIT,^
V + (V (1) - V) / 2.0 I ORIG VP,
RESUB 20#
V + (V (1) - V) / PP 20 I VP - V < 1.0*-3#
    ORIG VP I V, TRACE RAY (V, 0* R,, RSIGN, DSIGN), RECYCLE 20,^
TRACE RAY (V, 0* RP, DP, RPSIGN, DPSIGN),
P201#

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RP SIGN = RSIGN#*
CASE 1 FUNCTION (VP, V [1], RP, R [1], RPSIGN, RSIGN [1]*
VRR [2], VRR[3], RR[2], RR[3]),*
CASE 1 FUNCTION (V, VP, R, RP, RPSIGN, RSIGN*
VRR, VRR [1], RR, RR[1]), CASE 20 EXIT.
(*PAGE F 5276-4)
DSIGN = DSIGN [1]#
DSIGN = DPSIGN#
  PP20 * 2.0 | PP20, RESUB20.
  DPSIGN = 1#
    R SIGN = 1#
      PT0IPLUS20.
      PT0I20.^
    RSIGN = 1#
      PT0I20.
      PT0IPLUS20,000
  DPSIGN = RSIGN#
    P T0I20,
    PT0I PLUS 20,^
P TO I 20#
VP | V, RP | R, DPSIGN | DSIGN, RPSIGN | RSIGN, RECYCLE 20.
P TO IPLUS 20#
VP | V [1], RP | R [1], DPSIGN | DSIGN [1],
RPSIGN | RSIGN [1], RECYCLE 20,
CASE 20 EXIT.
(*PAGE F 5276-5)
CASE 31 FUNCTION (V(2), R(2), RSIGN(2), DSIGN(2), VRR(6), RR (6),
VP, RP, RPSIGN, DPSIGN, PP31,)^
+0 | VRR | VRR[1] | VRR[2] | VRR [3] | VRR [4] | VRR [5], 2.0 | PP31,
RECYCLE 31#
V{1} - V < 2.0*-2#
  CASE 1 FUNCTION (V, V[1], R, R[1], RSIGN, RSIGN[1]*
VRR, VRR [1], RR, RR [1]), CASE 31 EXIT.^
V + (V[1] - V) / PP31 | VP,
FIRST APPROX 31#
TRACE RAY (VP, 0^ RP, , RPSIGN, DP SIGN),
$RECEIVER RANGE ^ RP $ < 1.0 * -2#
PP31 + 1.0 | PP31, RECYCLE31,^
RP SIGN = R SIGN#
  P310,
  P311,
P310#
CASE 20 FUNCTION (V, VP, R, RP, RSIGN, RPSIGN, DSIGN, DPSIGN*
VRR, VRR[1], VRR[2], VRR[3], RR, RR[1], RR[2], RR[3]),
VRR=0#
  P TO I 31.
  CASE 1 FUNCTION (VP, V[1], RP, R[1], RPSIGN, RSIGN[1]*
VRR[4], VRR[5], RR[4], RR[5]), CASE31EXIT,
(*PAGE F5276-6)
P311#
CASE 20 FUNCTION (VP, V[1], RP, R[1], RPSIGN, RSIGN[1], DPSIGN, DSIGN[1]
|*
VRR [2], VRR [3], VRR [4], VRR [5], RR[2], RR[3], RR[4], RR[5]),
VRR[2] = 0 #
  P TO I IPLUS 131.
  CASE 1 FUNCTION (V, VP, R, RP, RSIGN, RPSIGN*, VRR, VRR [1], RR, RR [1]),
PTP62800
PTP62900
PTP63000
PTP63100
PTP63200
PTP63300
PTP63400
PTP63500
PTP63600
PTP63700
PTP63800
PTP63900
PTP64000
PTP64100
PTP64200
PTP64300
PTP64400
PTP64500
PTP64600
PTP64700
PTP64800
PTP64900
PTP65000
PTP65100
PTP65200
PTP65300
PTP65400
PTP65500
PTP65600
PTP65700
PTP65800
PTP65900
PTP66000
PTP66100
PTP66200
PTP66300
PTP66400
PTP66500
PTP66600
PTP66700
PTP66800
PTP66900
PTP67000
PTP67100
PTP67200
PTP67300
PTP67400
PTP67500
PTP67600
PTP67700
PTP67800
PTP67900
PTP68000
PTP68100
PTP68200
PTP68300
PTP68400

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CASE 31 EXIT.                                PTP68500
P T0 I 31Z                                PTP68600
VP I V, RP I R, DPSIGN I D SIGN, RECYCLE 31,   PTP68700
P T0 I PLUS 131#                            PTP68800
VP I V[1], RP I R[1], DPSIGN I DSIGN(1), RECYCLE 31.   PTP68900
CASE 31 EXIT#..,                            PTP69000
7                                              PTP69100
(*PAGE F 5529-1)                           PTP69200
(*THE FIRST SIX NAMES IN THIS DIMENSIONING STATEMENT
ARE USED BY THE PROGRAM AS THREE ORDERED PAIRS.)   PTP69300
TXATBNDRY =00,                                PTP69400
RCATRNDY = 00,                                PTP69500
TBIX INDEXTX = 00,                            PTP69600
RBIX INDEXRC = 00,                            PTP69700
TX SND SPD,                                PTP69800
RC SND SPD,                                PTP69900
B1:BNDRY 1 = 0000 ,                           PTP70000
B2:BNDRY 2 = 0000 ,                           PTP70100
INT=00,      NICHE = 00,      BOTTOM = 00,      TOP = 00,   PTP70200
,SHIFTED TABLE=000000,0000,   PTP70300
DEPTH = 000000,00000,   PTP70400
LEVEL,                                     PTP70500
SUDOR,                                     PTP70600
DEVICE 1 =00      ,DEVICE 2 = 00 ,   PTP70700
ABNE,                                     PTP70800
ATWG,                                     PTP70900
NEG2 = +2,0,                                PTP71000
WLOC,                                     PTP71100
ZEE=0*0,                                PTP71200
CEE = 0*0,                                PTP71300
STR,                                     PTP71400
STR1,                                     PTP71500
CNDX,                                     PTP71600
LIMIT,                                     PTP71700
IIL LIMIT = 00,                            PTP71800
      T TAB= 000000.00000 ,   PTP71900
TITLE FLAG.                                PTP72000
(*PAGE F 5529-2)
SEARCH# <NMRR OF A1S I IIL LIMIT;
INDEX INSTRUMENT LEVEL (ZSUBTX, IIL LIMIT, INDEXTX, TXATBNDRY),   PTP72100
INDEX INSTRUMENT LEVEL (ZSUBRC, IIL LIMIT, INDEXRC, RCATBNDRY),   PTP72200
COMPUTE INST C (ZSUBTX, INDEXTX, TX SND SPD),   PTP72300
PTP72400
TX SND SPD I TX SOUND SPEED,   PTP72500
COMPUTE INST C (ZSUBRC, INDEXRC, RC SND SPD).   PTP72600
PTP72700
0 I LEVEL,                                PTP72800
ZSUBTX = ZSUPRCX   PTP72900
      TX AT BNDY > 0#   PTP73000
      INDEXTX I B1 I B2, IIL LIMIT - 1 I LIMIT, CONTROL,   PTP73100
      SHIFT FOWN (INDEXTX, IIL LIMIT, 1), INDEXTX + 1 I INDEXTX I INDEXPTP73200
XRC I B1 I B2,   PTP73300
      ZSUBTX I DEPTH TABLE (INDEXTX), TX SND SPD I C (INDEXTX),   PTP73400
      IIL LIMIT I LIMIT + 1 I IIL LIMIT I NMRR OF A1S, CONTROL.**   PTP73500
(*PAGE F 5529-3)
ZSUBTX < ZSUPRCX   PTP73600
      INDEXTX I BNDY 1, INDEXRC I BNDY 2, 0 I DEVICE 1, 1 I DEVICE 2~   PTP73700
      INDEXRC I BNDY 1, INDEX TX I BNDY 2, 1 I DEVICE 1, 0 I DEVICE 2~   PTP73800
      TX AT BNDY (DEVICE 1) > 0#   PTP73900
      INDEXTX I BNDY 1, INDEXRC I BNDY 2, 0 I DEVICE 1, 1 I DEVICE 2~   PTP74000
      INDEXRC I BNDY 1, INDEX TX I BNDY 2, 1 I DEVICE 1, 0 I DEVICE 2~   PTP74100

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TX AT BNDRY [DEVICE 2] > 0x0 PTP74200
SHIFT DOWN (B2, IIL LIMIT, 1^), INDEXTX [DEVICE 2] + PTP74300
1 I B2 I INDEXTX [DEVICE 2], ZSUTX [DEVICE 2] I PTP74400
DEPTH TABLE (B2), TX SND SPD [DEVICE 2] I C (B2), PTP74500
IIL LIMIT I LIMIT + 1 I IIL LIMIT I NMRR OF A1S PTP74600
IIL LIMIT - 1 I LIMIT, CONTROL.^ PTP74700
TX AT BNDRY [DEVICE 2] > 0x0 PTP74800
SHIFT DOWN (B1, IIL LIMIT, 1^), B1 + 1 I B1 I INDEXTX [DEVICE 1], PTP74900
INDEXTX [DEVICE 2] + 1 I B2 I INDEXTX [DEVICE 2], PTP75000
ZSUBTX [DEVICE 1] I DEPTH TABLE (B1), PTP75100
TX SND SPD [DEVICE 1] I C (B1), IIL LIMIT I LIMIT + PTP75200
1 I IIL LIMIT I NMRR OF A1S PTP75300
SHIFT DOWN (B2, IIL LIMIT, 2^), B2 I SUDOR + 2 I B2 I INDEXTX [DEVICE PTP75400
E 2], PTP75500
ZSUBTX [DEVICE 2] I DEPTH TABLE (B2), PTP75600
TX SND SPD [DEVICE 2] I C (B2), IIL LIMIT + 1 I LIMIT + 1 I IIL LIMIT PTP75700
T PTP75800
I NMRR OF A1S, PTP75900
SHIFT DOWN (B1, SUDOR, 1^), B1 + 1 I B1 I INDEXIX [DEVICE1], PTP76000
ZSUBTX [DEVICE 1] I DEPTH TABLE (B1), TX SND SPD [DEVICE 1] I C (B1) PTP76100
PPTP76200
(*PAGE F 5529-4)
CONTROL# C I STR, CNDX = 0 (1) NMRR OF A1S = 1 +C (CNDX + 1) I STR1 > SPTP76400
PTP76500
TR#
STR1 I STR I CMAX TABLE[CNDX], DEPTH TABLE [CNDX+1] I CMXZTAB [CNDX] PTP76600
PTP76700
STR I CMAX TABLE[CNDX], STR1 I STR, DEPTH TABLE [CNDX] I CMXZTAB [CNDX] PTP76800
DX)^
BNDRY 1 = 0x0 PTP76900
0 I MAX V ON PROFILE, ST LOOP2.^ PTP77000
ST LOOP1# C I MAX V ON PROFILE, 0 I TITLE FLAG, PTP77100
LOOP 1# LEVEL < BNDRY 1# PTP77200
SEARCH MAX V ON PROFILE, LOOP1.^ PTP77300
ST LOOP2# C I LEVEL) I INITIAL VELOCITY, PTP77400
LOOP2# LEVEL = LIMIT#
INITIAL VELOCITY > MAX V ON PROFILE PTP77500
INVZ I MAX PROFILE DEPTH, PTP77600
INITIAL VELOCITY I MAX V ON PROFILE FOR SEARCH MAX V ON PROFILE, PTP77700
EXIT SEARCH,^ PTP77800
LEVEL = BNDRY 2# PTP77900
SEARCH INITIAL VELOCITY , LOOP2, PTP78000
INITIAL VELOCITY > MAX V ON PROFILE# PTP78100
INVZ I MAX PROFILE DEPTH, PTP78200
INITIAL VELOCITY I MAX V ON PROFILE# PTP78300
LOOP 3# LEVEL > LIMIT# PTP78400
SEARCH MAX V ON PROFILE, LOOP3. EXIT SEARCH# PTP78500
PTP78600
(*PAGE F 5529-5)
INDEX INSTRUMENT LEVEL (DEPTH OF INSTR. LIMIT, INDEX, AT BNDRY, LMFLT,) PTP78900
# -FX TO FL (LIMIT# LMFLT), LMFLT = DEPTH OF INSTR / (DEPTH TABLE [LIMIT] PTP79000
TI - DEPTH TABLE) I INDEX,
FL TO FX (INDEX# INDEX),
INDEX > LIMIT#
LIMIT I INDEX# PTP79100
INDEX = 0# PTP79200
LOOP,^ PTP79300
LP# DEPTH TABLE [INDEX] = 0# PTP79400
INDEX - 10 I INDEX, INDEX > 0# PTP79500
PTP79600
PTP79700
PTP79800

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LP,
  0 | INDEX, LOOP,^
  LS00PZ INDEX > LIMITZ
    ->PRINTER <> << THE $INSTRUMENT $ LEVEL $ IS $ GREATER $ THAN$ THE $PTP80200
      VALUESSINSTHE$DEPTH$TABLE.>> + NEXT TRG,^
  LS0PZ DEPTH TABLE [INDEX] = DEPTH OF INSTRZ
    1 | AT BNDRY, EXIT IIL.^
DEPTH TABLE [INDEX] < DEPTH OF INSTRZ
  DEPTH OF INSTR < DEPTH TABLE [INDEX + 1]^
    -1 | AT BNDRY, EXIT IIL.^
    INDEX + 2 | INDEX, LOOP,^
    INDEX + 1 | INDEX, LOP. EXIT IIL^ + SETOPZ.., PTP81000
7^ PTP81100
(*PAGE F 5520+6) PTP81200
COMPUTE INSTC (ZEE, INDEX, INSTC, WKLC,)^ + INDEX = NMNR OF A1S^ PTP81300
(*CHECK IF @1 BOTTOM) INDEX = 1 | INDEX^ PTP81400
ZEE + ZEE + A1TABLE [INDEX] + ZEE + A2 TABLE [INDEX] + A3 TABLE [INDEX] PTP81500
| WKLC, 1.0 / WKLC | WKLC, PTP81600
SQRT (WKLC^ INSTC)^ PTP81700
SHIFT DOWN (TOP, BOTTOM, INT, NICHE,)^ PTP81800
  * PTP81900
    DEPTH TABLE[82] | D TAB , PTP82000
    RDEPTH | DEPTH , PTP82100
    NICHE = BOTTOM (-1) TOP + PTP82200
    DEPTH TABLE[NICHE] | D TAB , DEPTH TABLE[NICHE+INT] | SHIFTED TABLE, PTP82300
    DEPTH TABLE [NICHE] | DEPTH TABLE[NICHE + INT], PTP82400
    C [NICHE] | C [NICHE + INT], PTP82500
    A1 TABLE [NICHE] | A1 TABLE [NICHE + INT], PTP82600
    A2 TABLE [NICHE] | A2 TABLE [NICHE + INT], PTP82700
    A3 TABLE [NICHE] | A3 TABLE [NICHE + INT]^ PTP82800
(*PAGE F 5529-7) PTP82900
SEARCH MAX V ON PROFILE^ +A1 TABLE [LEVEL] | ACNE < 0^ PTP83000
  SEARCH MV,^ PTP83100
COMPUTE MVZ A2 TABLE [LEVEL] | ATW0 / NEG2 / ACNE + ZEE, PTP83200
  DEPTH TABL [LEVEL] < ZEE < DEPTH TABLE [LEVEL] + 1^ PTP83300
    ZEE + ZEE + ACNE + ZEE + ATW0 + A3 TABL [LEVEL] + WLOC, PTP83400
    1.0 / WL0F + WL0C, SQRT (WL0C^ CEE), PTP83500
    CEE > CMX TABLE [LEVEL]^ PTP83600
      CEE | CMXTABLE [LEVEL], ZEE | CMXTAB[LEVEL], PTP83700
      TITLE FLAG = 0^ PTP83800
      1TITLE FLAG,->PRINTER<>,<<CMAX?>CFE<?Z(CMAX)?>ZEE>^ PTP83900
      ,*PRINTER<?&SSCEE??&SSZEE>***** PTP84000
SEARCH MV^ PTP84100
CMXTABLE [LEVEL] > MAX VON PROFILE^ PTP84200
  CMXTABLE [LEVEL] | MAX VON PROFILE, PTP84300
  CMXTAB [LEVEL] | MAX PROFILE DEPTH^ PTP84400
SET MV^ LEVEL + 1 | LEVEL^ PTP84500
(*PAGE F5529-8) PTP84600
SEARCH INITIAL VELOCITY^ +A1 TABLE [LEVEL] | ACNE < 0^ PTP84700
  SEARCH IV,^ PTP84800
COMPUTE IV^ A2 TABLE [LEVEL] | ATW0 / NEG2 / ACNE + ZEE, PTP84900
  DEPTH TABLE [LEVEL] < ZEE < DEPTH TABLE [LEVEL] + 1^ PTP85000
    ZEE + ZEE + ACNE + ZEE + ATW0 + A3 TABL [LEVEL] + WLOC, PTP85100
    1.0 / WL0F + WL0C, SQRT (WL0C^ CEE), PTP85200
    CEE > CMXTABLE [LEVEL]^ PTP85300
      CEE | CMXTABLE [LEVEL], ZEE | CMXTAB [LEVEL], PTP85400
      TITLE FLAG = 0^ PTP85500

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1 I TITLE FLAG, +PRINTER <>,,<<CMAX?>CFF<?Z(CMZX)?>ZEE>;n PTP85600
,+PRINTER <$$$$%CFE??$%ZFE>;n~~~~~ PTP85700
SEARCH IVZ CMAX TABLE [LEVEL] > INITIAL VELOCITY#
CMAXTABLE [LEVEL] I INITIAL VELOCITY,
CMXZTAB [LEVEL] I INVZ~~ PTP85800
SET IVZ LEVEL + 1 I LEVEL.. PTP85900
PTP86000
PTP86100
```